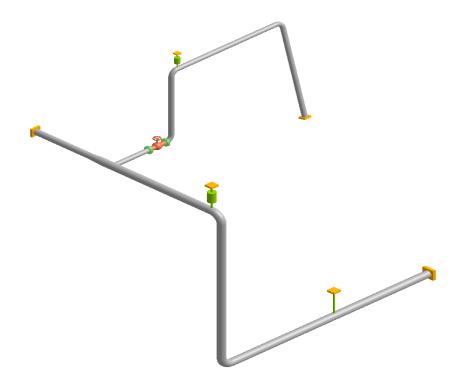
CAEPIPE[™]

Tutorial for Modeling and Results Review Problem 2





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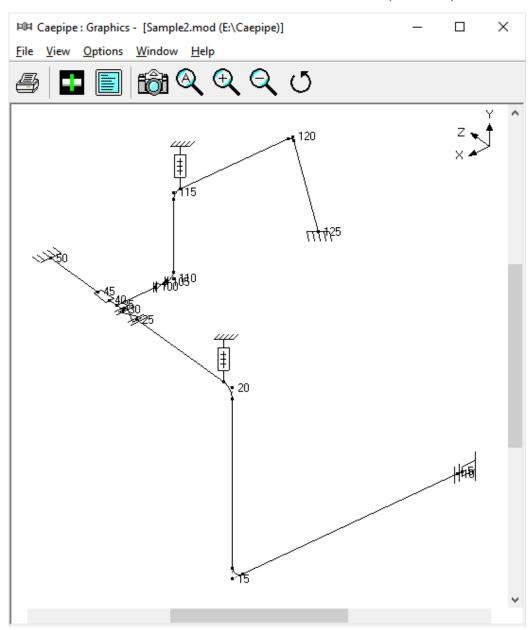
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Modeling and Results Review - Problem 2

Let us model a slightly more advanced piping system now that you have familiarized yourself with the basic use of CAEPIPE via Tutorial 1. The details of the model (in SI units) are shown below:



You will learn how to:

- 1. Enter Title
- 2. Select Analysis options (piping code etc.)
- 3. Define Material, Section and Loads for the model
- 4. Input Model Layout (different loads for different segments)
- 5. Select Load Cases for Analysis
- 6. Analyze
- 7. View Results

Modeling and Results Review - Problem 2

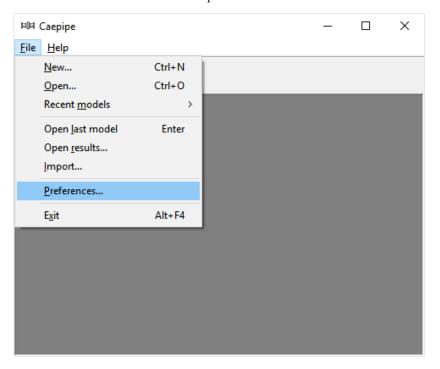
Model Description

Details of the Layout, Material, Sections, Loads and Connection details are summarized for reference:

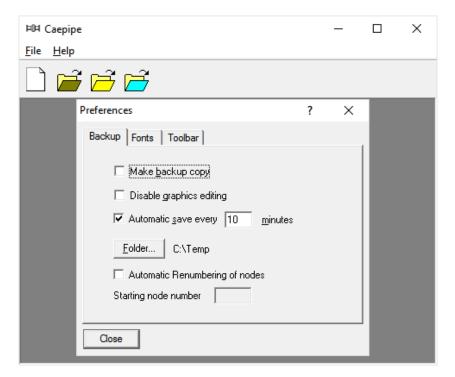
- 1. **Axes Chosen:** Global X = East, Global Y = Up and Global Z = South
- 2. **Piping Code:** ASME B31.1 (2014)
- 3. Section Properties:
 - a. Main Line: 10" Schedule STD
 - b. Branch Line: 6" Schedule STD
- 4. Insulation throughout the Piping system:
 - a. **Density**: 176.2 kg/m3
 - b. **Thickness**: 65 mm
- 5. **Material**: A 312 TP 316
- 6. Temperature:
 - a. For Main Line and Branch Line up to Valve End Node 105: 185 Deg. C
 - b. For Branch Line after Valve Node 105: 260 Deg. C
- 7. Pressure:
 - a. For Main Line and Branch Line up to Valve End Node 105: 10 bar
 - b. For Branch Line after Valve Node 105: 32 bar
- 8. Operating Fluid and Specific Gravity: Steam, 0.1
- 9. Connection Details:
 - a. Node 5 connecting to Nozzle of a Cylindrical Vessel
 - b. Node 55 connecting to Nozzle of a API 610 Horizontal Pump
- 10. Wind Velocity: 100 km/hr
- 11. **Static Seismic g's**: X=0.3, Y=0.2 and Z=0.3

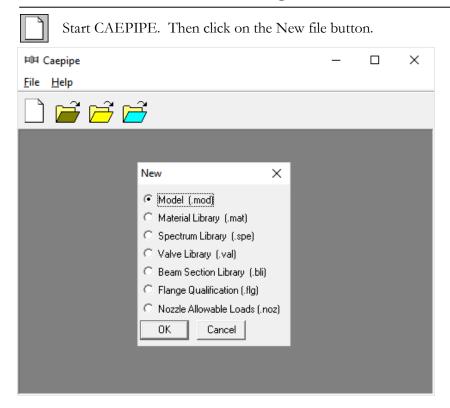
Modeling and Results Review - Problem 2

Start CAEPIPE. From the File pull down menu select Preferences.



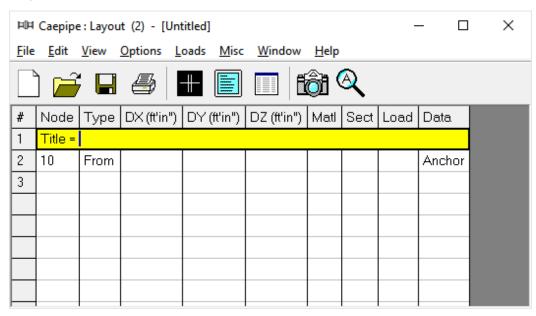
Make sure that the Automatic save feature is enabled and the Automatic Renumbering of nodes feature is disabled.



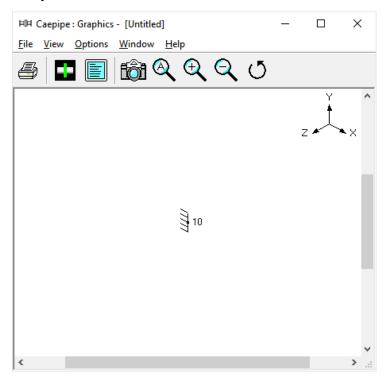


From the New file dialog, select the type of the new file as Model (.mod) file. This opens two independent windows: Layout and Graphics.

Layout window



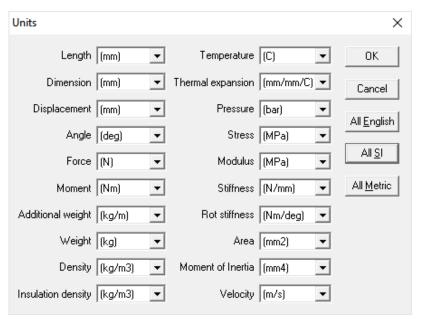
Graphics window



Adjust the size of the windows to fit your desktop such that you can view both comfortably at the same time.

Change Units

As this is an SI/Metric model, change the units appropriately. From the layout window, click on Options menu > Units (alternately, press the hotkey Ctrl+U). Click on "All SI" button followed by OK. The layout window will show the offsets (DX/DY/DZ) in mm units.

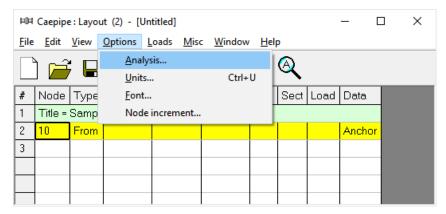


1. Enter Title

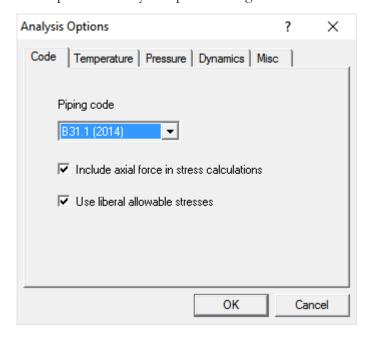
Type "Sample Problem 2" as the title in the first row that contains "Title = ". Press Enter.

2. Select Analysis options (piping code etc.)

Click on the Options menu and then select Analysis (Options > Analysis) to specify options for analysis.



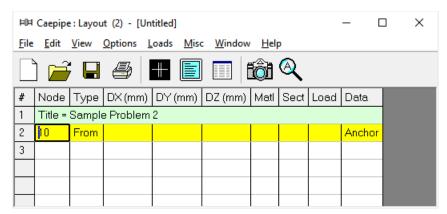
This opens the Analysis Options dialog.



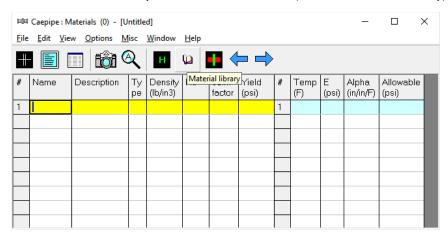
On the Code property page, select B31.1 (2014) for Piping code. Turn ON the options "Include axial force in stress calculations" as well as "Use liberal allowable stresses". Then click on OK to close Analysis Options dialog.

3. Define Material, Sections and Load

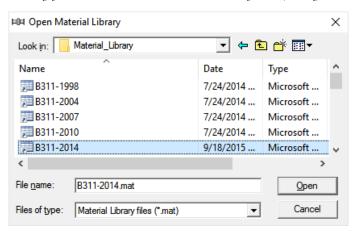
Click on "Matl" in the header in the Layout window (or press Ctrl+Shift+M)



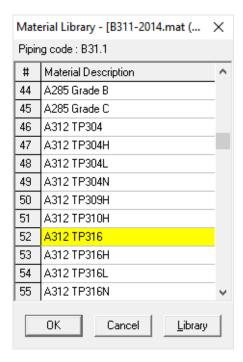
This opens up the Materials list in a separate List window. Position and resize the list window as you desire. Click on Library button on the Toolbar (or choose File > Library).



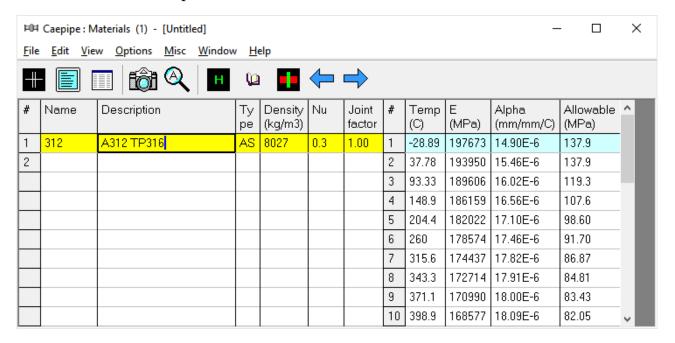
The Open Material Library dialog is shown. If you don't see the folder, shown below, then navigate to the Material Library folder under the CAEPIPE installed folder (usually C:\CAEPIPIE\xxx, xxx = version number).



Select B311-2014.mat as the library file by double clicking on it. The available materials in the library are shown. Scroll down to A312 TP 316. Double click on it or click on OK to select it.

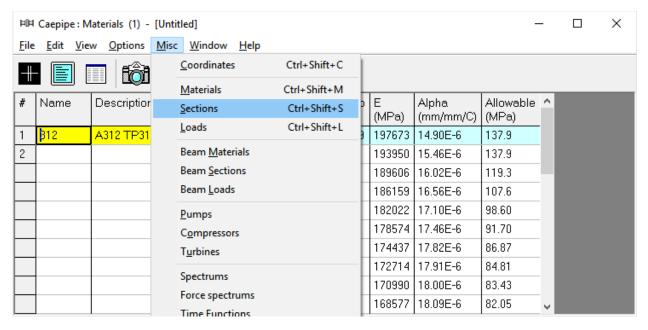


The properties for this selected material are transferred to the material in the List window. Type "312" for material name and then **press Enter**.

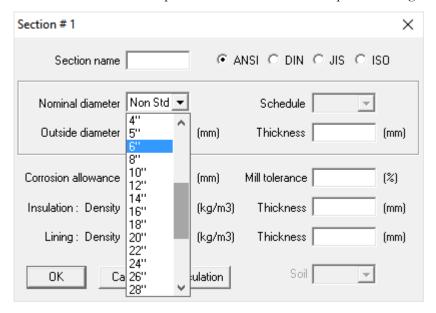


Sections

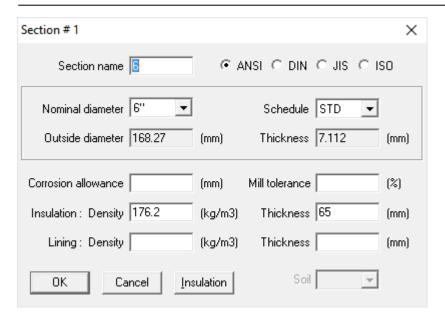
Select Sections from the Misc menu of the List window (or press Ctrl+Shift+S).



A list of Sections is shown. This system has three sections: 6", 8" and 10". To enter the first section, type '6' for Section name and press Enter. The Section Properties dialog is shown with the section name 6.



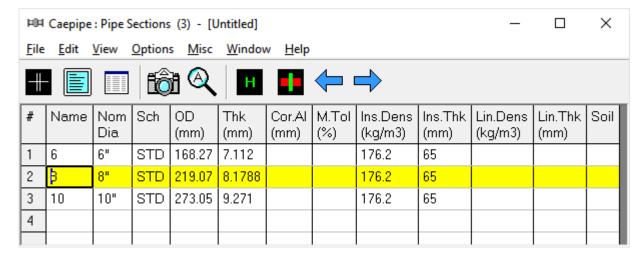
Click on the down arrow of the dropdown combo box for Nominal diameter and select 6" for Nominal diameter. Select/Enter other properties (STD thickness, Insulation density [Alt+I may be used for a list of insulation materials or you may enter your own density, in this case, 176.2 kg/cu.m] and thickness).



After entering all properties, press Enter or click on OK to enter the first section.

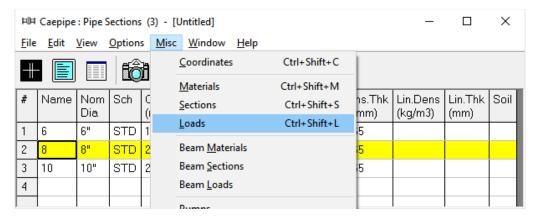
Now repeat the process for the 8" pipe section.

In row # 2, Type 8 for Section name and press Enter. The Section Properties dialog is shown with the section name 8. Select 8" for Nominal diameter, STD for Schedule, and same insulation properties as before for Insulation. Press Enter or click on OK to enter the second section. Do similarly for the 10" pipe section.

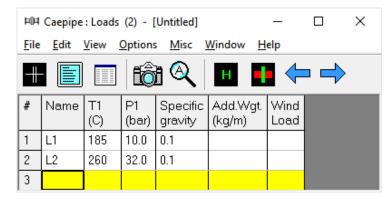


Load

Select Loads from the Misc menu (or press Ctrl+Shift+L).



The Loads list is shown. To enter the first load, Type 'L1' for Name, Tab to T1 and type 185, Tab to P1 and type 10 bar, Tab to Specific gravity and type 0.1. Then press Enter. That is it! The load is entered. (Alternately, you could have pressed Ctrl+E on the first row and typed in the same information in a dialog box). Similarly, enter the second load set "L2" {260°C, 32 bar, Sp. Gravity = 0.1}.



Click in the Layout window or press F3 to move the focus to the Layout window.

4. Input Model Layout

We are going to model the 10" main line first, followed by the 8" segment.

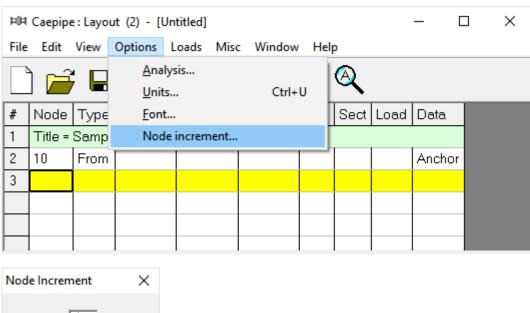
CONVENTIONS

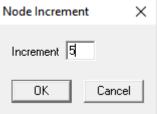
- In the following text, the word 'type' should be distinguished from the words 'Type column' or simply 'Type' (upper case 'T'). The former ('type') will mean press the keys on the keyboard. The latter word 'Type' will refer to the Type column in the Layout spreadsheet. Of course, occurrence of Type at the beginning of a sentence will mean "type" the keys.
- Also, the instruction "type B for Bend" does not necessarily mean the upper case B'. The lower case b' can also be typed.
- For items in the Data column (such as Anchor or Hanger), the cursor needs to be in the Data column. To move the cursor quickly to that column, press Ctrl+D from any column or click in the Data column. Or press the Tab key repeatedly to reach the Data column.

- As the graphics window is simultaneously updated, you should position the graphics window in such a
 way that you can see it along with the input window. Simultaneous feedback is one of the chief design
 intents in CAEPIPE.
- For mouse clicks, when you read the word "click on xxx," this means left-click on your mouse. For the context menu, if referred to, right-click.

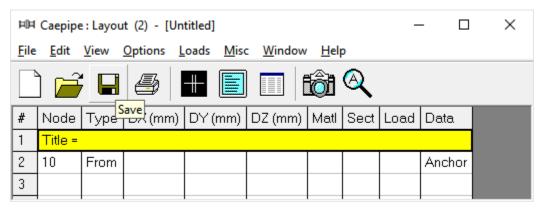
Change Node Increment

You might have noticed in the model drawing that the node numbering scheme has an increment of 5. CAEPIPE has a feature that allows you to specify a node increment. Select Options menu > Node increment...type 5 for value. Click on OK.

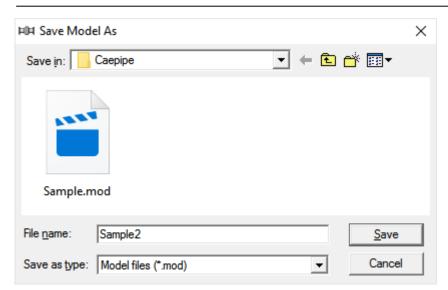




After defining the above parameters, Save the model by clicking on the Save button.



The "Save Model As" dialog is shown.



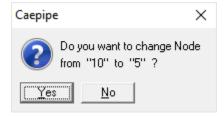
Type the File name as "Sample2" and press Enter to save the model.

First model the 10" Main line

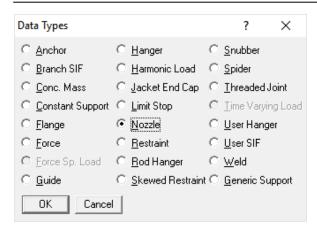
Following the Title at row #1, row #2 is already generated with Node 10 of Type "From" with an Anchor in the Data column.

Model information shows that the piping is connecting to a Nozzle of a Cylindrical Vessel with node number as 5. So, to account for the stiffness of the Nozzle protruding out of the Cylindrical Vessel, the nozzle portion is modeled as a pipe in this model. The junction of this Pipe (Nozzle) and the Shell is modeled as "Nozzle".

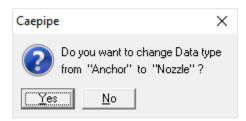
To change the Node number and to replace "Anchor" with "Nozzle", click on 10, press Backspace to erase 10, type 5. Press Tab to advance. Confirm the node number change when asked (by clicking on Yes, or simply pressing the Spacebar key on the keyboard).



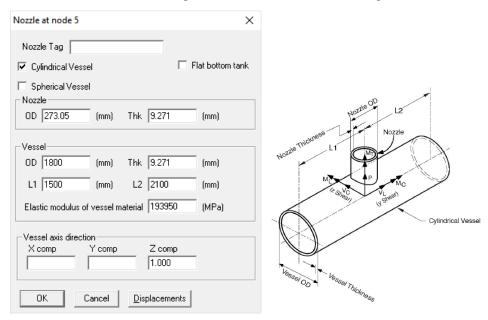
To replace the "Anchor" with "Nozzle", highlight the data type "Anchor" at row #2 using mouse left button and then click on "Data" in the header in the Layout window. From the "Data types" dialog box shown, select the new data type as "Nozzle".



CAEPIPE will prompt as shown below. Press "Yes" to proceed.

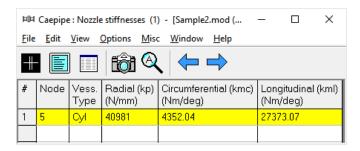


Enter the Nozzle and Vessel parameters as shown below and press "OK".

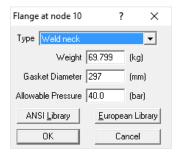


From the snap shots shown above, Lengths L1 and L2 on either side of the nozzle are the distances from the nozzle center line to the nearest location on vessel where the "ovalization deformation" of the vessel is stopped such as at a stiffener on the inner or outer surface of the vessel, or at the center of a saddle support to the vessel or at the junction to the torispherical enclosure (also called the head) or at a tube sheet inside the vessel etc.

Nozzle stiffness computed by CAEPIPE can be seen through Layout window > View > List > Nozzle Stiffnesses.

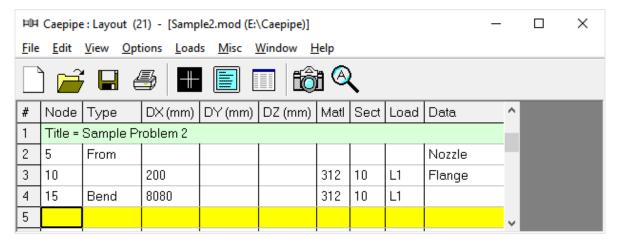


Now, press Enter to move the highlight to the next row (#3). Tab to the Type column. The next Node 10 is automatically assigned. Tab over to DX, type 200 (mm), Tab over to Material, press Enter to open the list of materials and select 312. Next Tab over to Section and press Enter. Select section 10 and press OK. Tab over to Load and press Enter, select L1 and click OK. Tab again to Data to input the flanges mating with the pipe and the equipment nozzle. Type "fl" to model flange and enter the data as shown below and press OK. CAEPIPE moves the highlight automatically to the next (new) row (#4).

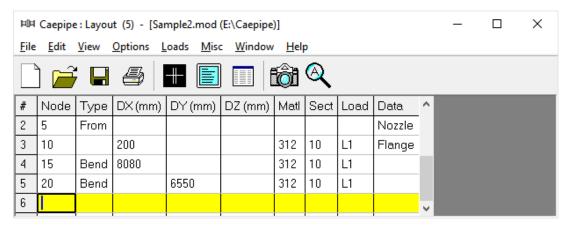


Tab to the type column. The next node 15 is automatically assigned.

Node 15 has a LR (long radius) bend (in CAEPIPE, a bend node is defined always at the tangent intersection point, being such, this node does not exist on the physical bend). Press Tab to go the Type column; type "ben" to insert a default LR bend. Tab to DX, type in 8080 (mm), press Enter. CAEPIPE automatically enters the material, section and load from the previous row and moves the highlight to the next new row.

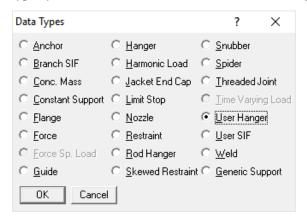


The following vertical bend (at node 20) can be modeled as before. Tab to Type (node 20 is automatically inserted), and type "ben" to insert a default LR bend, Tab again to DY, type 6550 (mm) and press Enter.

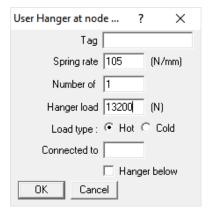


This bend has an already existing hanger (called "User Hanger" in CAEPIPE) at the far end, referred to as node 20B, an internally generated bend node.

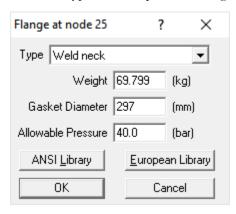
So, on the next row, type 20B, Tab to Type, press "L" for Location, which spawns the available data types you can insert at this node. Pick "User Hanger" from the dialog.



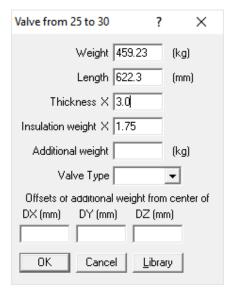
Enter its properties as shown. Click on OK.

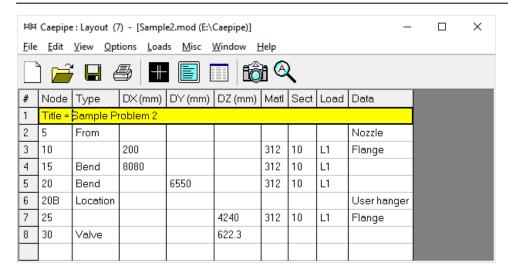


Next, the line moves in the Z direction to the flange node 25. Pressing Tab on the new row generates node 25 for you. Tab to DZ, type 4240, (click in Data column) or press Ctrl+D to move cursor to Data column. Type "fl" to open the Flange Data type dialog. Enter the details shown below and press OK.

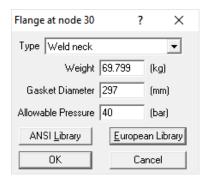


A valve is placed next from Node 25 to Node 30, where another mating flange is located. Pressing Tab on the new row generates node 30. Press Tab to go the Type column; type "v" to insert a "Valve" and enter the data as shown below and press OK.

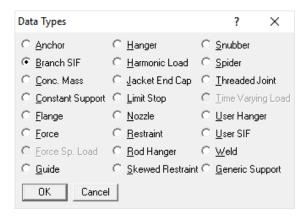


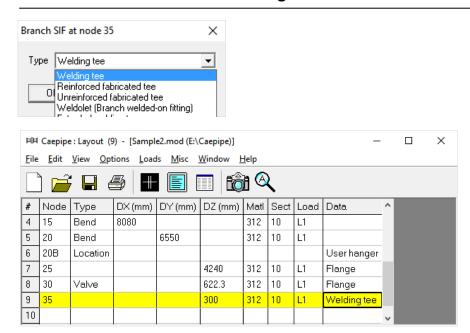


Tab to Data and type "fl" to enter a "flange". Type "fl" to open the Flange Data type dialog. Enter the details shown below and press OK.



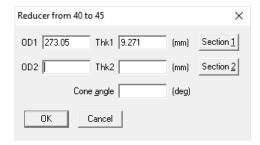
Next model a pipe element till node 35 (welding tee). Press Tab for node 35, Tab to DZ, type 300, (click in Data column) or press Ctrl+D to move cursor to Data column. Type "br" (or right-click in Data, select Branch SIF) to open the Tee types Data type dialog. Select Welding Tee from the dropdown box. Click on OK (or press Enter).



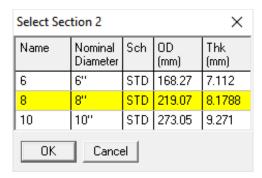


Next model a pipe element till node 40. Press Tab for node 40, Tab to DZ, type 300 and press Enter.

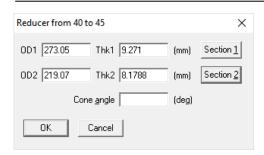
The next element is a 10x8 concentric reducer. Here is how to model it. Tab for the next node # (45), type "red" for Reducer in the Type column. CAEPIPE displays the Reducer dialog with the current section properties.



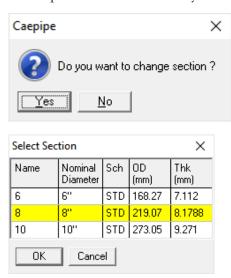
Click on "Section 2" button to select the following section, in this case, the 8" section. After placing the highlight on the 8" section, press Enter (or click on OK).



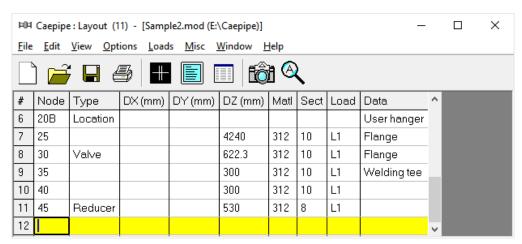
You are back at the Reducer dialog.



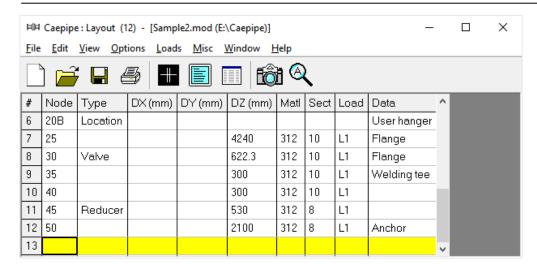
Click on OK to finish inserting the reducer. On the layout screen, type 530 for DZ and press Enter, at which point CAEPIPE wants you to confirm the section change. Click on Yes.



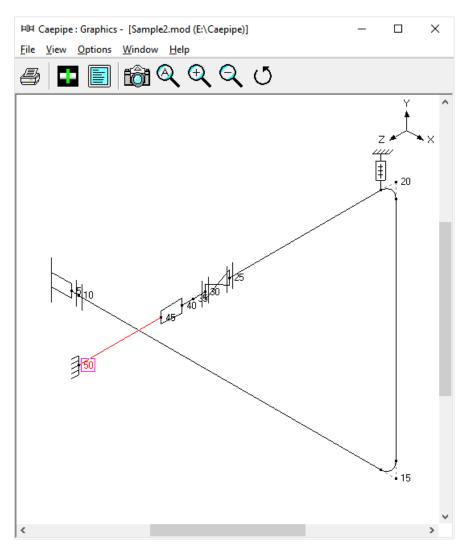
Then select 8 as the new section from here on. Press Enter to move to next row.



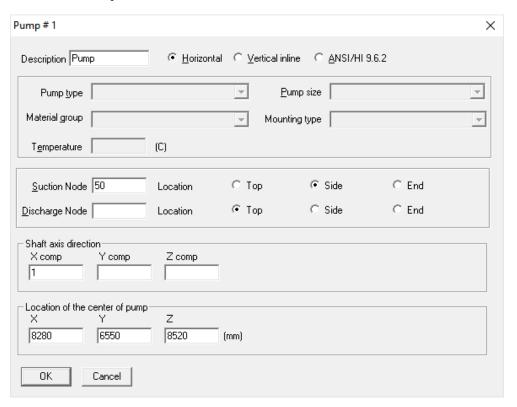
The last element here is an 8" pipe that ends at node 50. As before, press Tab for 50, type 2100 for length in the same direction. Press Ctrl+D to go to Data and press A to insert a rigid anchor (note that CAEPIPE inserts the correct old material, new section and old load for this row).



Click on the Zoom All button (or press Ctrl+A) to view the header line fully in the graphics window.

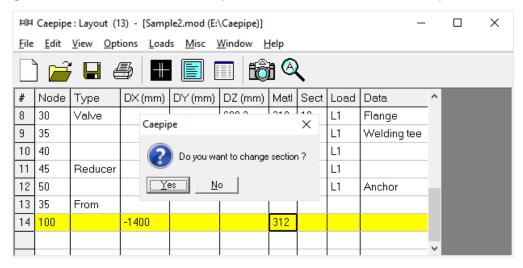


Node 50 is connecting to a Side Suction Nozzle of an API 610 Horizontal Pump. To model this, select the option "Pumps" through Layout Window > Misc. Double click on an empty row and enter the values as shown below. Once modeled, CAEPIPE will automatically perform the Pump Qualification and shows the report in Results.

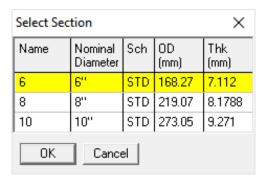


Now the 6" branch

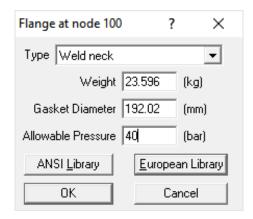
On the next row (#13), type 35 for Node, Tab to the Type column, type 'f' (for "From", since we are beginning a new branch from an existing Node 35), press Enter. In the next row (#14), type "100" in the Node column to clearly identify the new branch. Tab to DX and enter –1400. CAEPIPE inserts the previous material, and automatically detects the new branch and asks if you want to change section.



Since we want to change the section to 6, click on Yes. This opens the Section selection dialog.

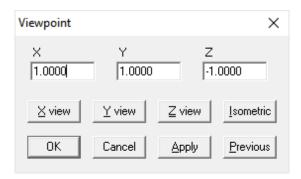


Select the 6" section by double clicking on it. The section (6) is entered in the Section column in the Layout window. The load is again automatically inserted from the previous load. Lastly, type "fl" in the Data column and hit enter to create a mating Flange. This will bring up the Flange type dialog box.

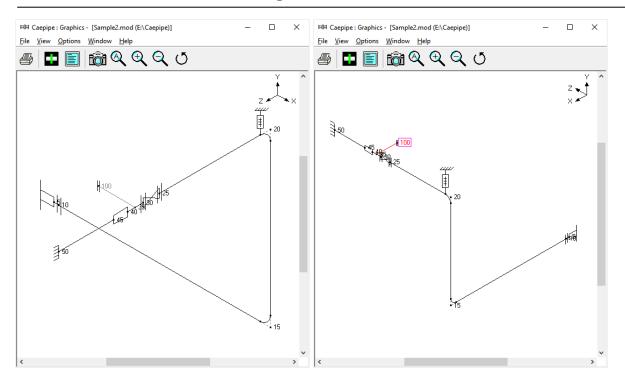


Type in 23.596 for Weight, 192.02 for Gasket Diameter, 40 for Allowable Pressure and click Ok.

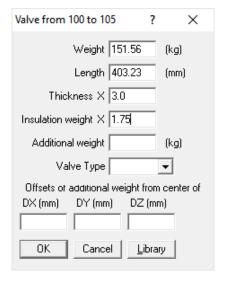
The graphics window will look like this. For better view, rotate the model by clicking the icon and scrolling the horizontal scroll bar towards left using the mouse left button or through keyboard left arrow key. Alternatively, you can specify the viewpoint as shown below by selecting the icon from the



graphics frame.



In the next row (#15), Tab to the Type column. The next Node 105 is automatically assigned. In the Type column, type 'v' (for Valve). This brings up the Valve dialog box.

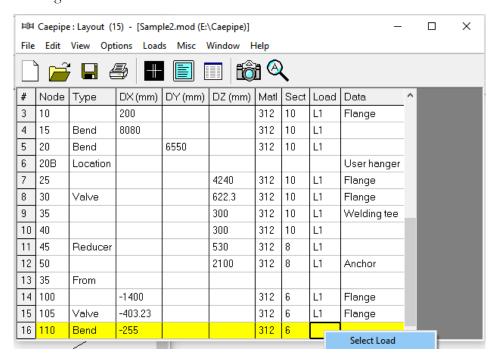


In the Valve dialog box, type 151.56 for Weight, 403.23 for Length, 3.00 for Thickness, and 1.75 for Insulation weight. Then press Enter or click on OK to input the valve. Press Enter again. You will see that the DX, Material, Section and Load information is automatically input in the Layout window.

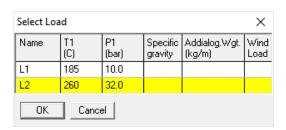
You can now copy the flange along with data from Node 100 and paste it at Node 105. To perform this, highlight row # 14 and press Ctrl+C. Then move the cursor to data column of row #15 and press Ctrl+V to paste the flange. Press Enter to move to the next row.

ÞÞ	FIII Caepipe: Layout (15) - [Sample2.mod (E:\Caepipe)]											
<u>F</u> ile	<u>E</u> dit	<u>V</u> iew <u>O</u> pt	ions <u>L</u> oad	s <u>M</u> isc <u>\</u>	<u>W</u> indow <u>F</u>	<u>l</u> elp						
#	Node	Туре	DX (mm)	DY (mm)	DZ (mm)	Matl	Sect	Load	Data	^		
3	10		200			312	10	L1	Flange			
4	15	Bend	8080			312	10	L1				
5	20	Bend		6550		312	10	L1				
6	20B	Location							User hanger			
7	25				4240	312	10	L1	Flange			
8	30	Valve			622.3	312	10	L1	Flange			
9	35				300	312	10	L1	Welding tee			
10	40				300	312	10	L1				
11	45	Reducer			530	312	8	L1				
12	50				2100	312	8	L1	Anchor			
13	35	From										
14	100		-1400			312	6	L1	Flange			
15	105	Valve	-403.23			312	6	L1	Flange			
16										v		

In the next row (#16), Tab to the Type column, type "b" to create a Long Radius Bend and then Tab to the DX column. The default LR Bend is automatically input when you Tab over. In the DX column type –255 and hit Enter. The Material, Section and Load information and is automatically input. As the Temperature and Pressure is changing from this element, change the Load from L1 to L2 by right clicking on the "L1" in the Load field.

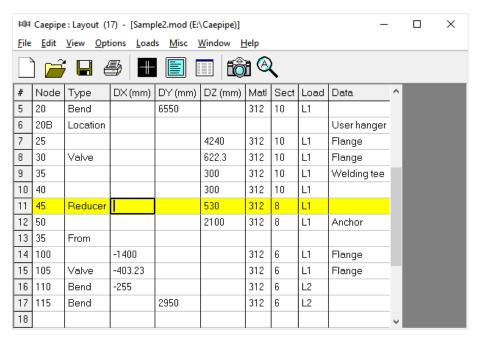


This will bring up a small Context menu from which you will choose Select Load. This will bring up the Select Load window. Highlight L2 and click Ok. Press Enter to complete inputting Node 110 at row (#16).

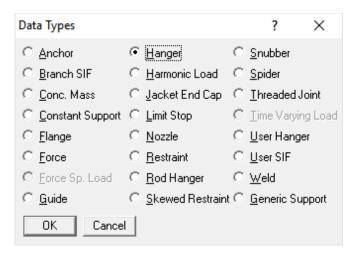


In the next row (#17), create another Long Radius Bend just like the one in row (#17), except change the DX -255 to DY 2950 and press Enter.

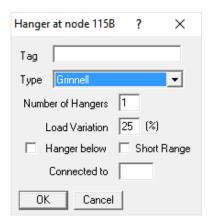
Your Layout window should look like this.



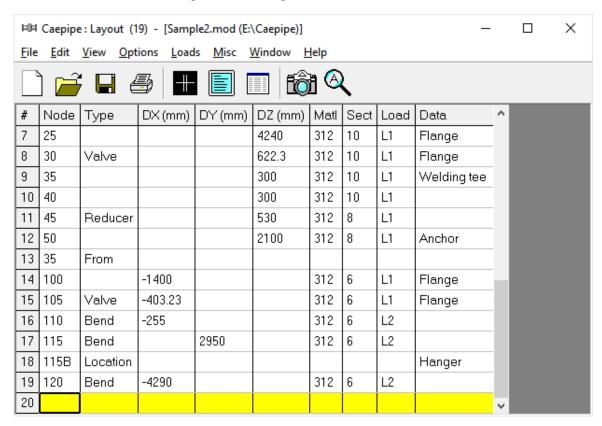
Start the next row (#18) by typing 115B in the Node column. Tab to the Type column and type "L" to specify a Location type. This will automatically open the Data Types dialog box. Select Hanger.



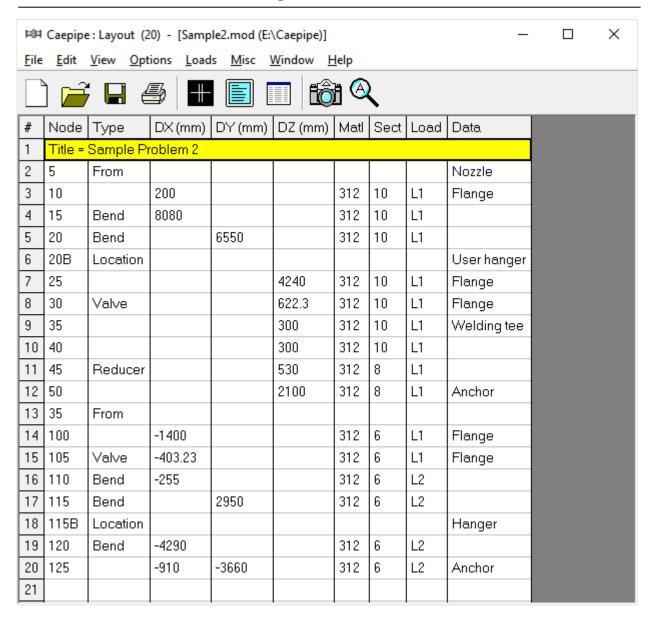
Another dialog box will appear with specific Hanger type input options. Keep the default settings and click OK.



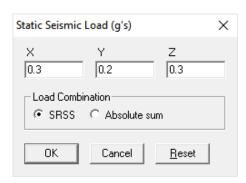
In Node 120 on the next row (#19), Tab to the Type column and input a default LR Bend by typing "b". Tab to the DX column and input –4290 and press Enter.



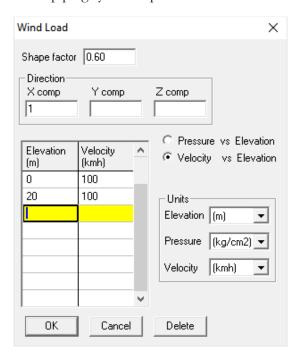
On the next row (#20), Tab over to the DX column and input -910, then in DY input -3660. Create an Anchor in the Data column by either pressing Ctrl+D or Tabbing to the Data column and typing "a". Press Enter and you are done with Layout window input.



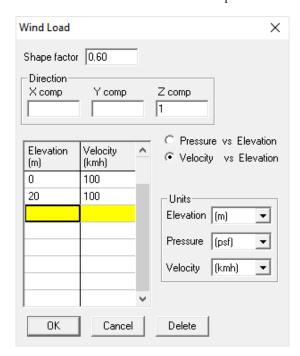
Define "Static seismic" through Layout Window > Loads > Static Seismic. Enter the value as show below.



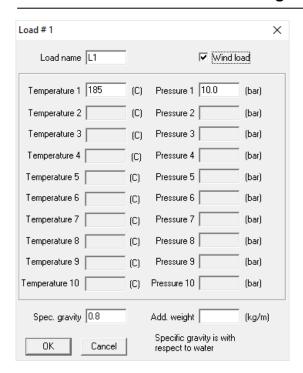
Let us define "Wind Load" profile in +X direction through Layout Window > Loads > Wind 1 and enter the data as shown below and press OK. The maximum elevation of 20m is chosen so that the entire piping system experiences the wind loads.



Similarly, define "Wind Load" profile in +Z direction through Layout Window > Loads > Wind 2 and enter the data as shown below and press OK.



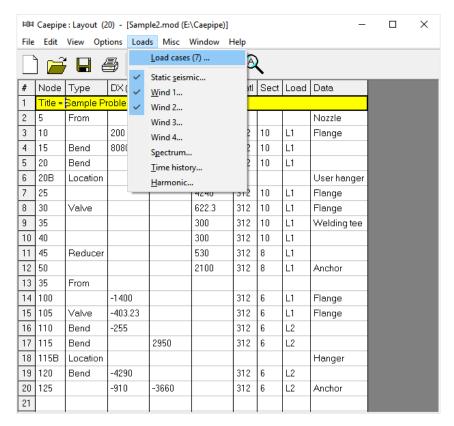
Assign the Wind Loads defined above to the stress layout through Layout window > Misc > Loads and then double on the Loads "L1" and select the check box "Wind load" as shown below.



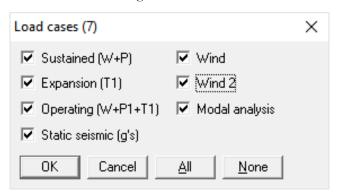
Similarly, select the check box "Wind load" for "L2".

5. Select Load Cases for Analysis

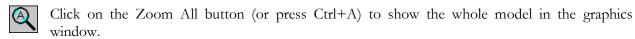
Select Loads cases from the Loads menu.

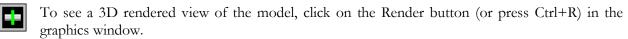


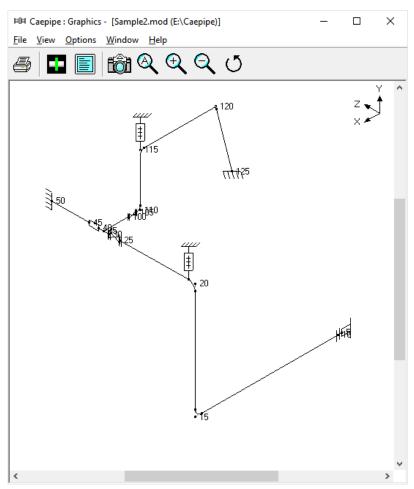
The Load cases dialog is shown.

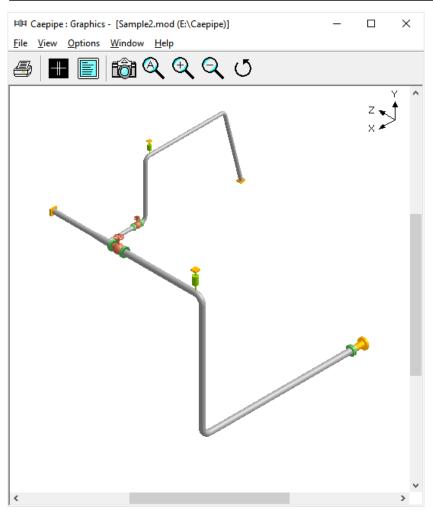


By default, Sustained (W+P), Expansion (T1) and Operating (W+P1+T1) load cases are already selected. Add Static Seismic (g's), Wind, Wind 2, and the Modal analysis Load cases by clicking on the checkbox next to it and press OK to return to the Layout window. The model input is now complete.







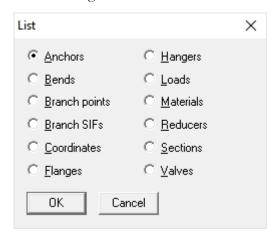


#

To return to the non rendered view, click on the Do not render button (or press Ctrl+R).

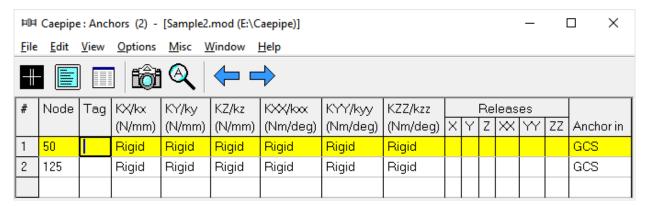
List

One of the useful features of CAEPIPE is the ability to show a list of all like items such as anchors, bends etc. in a separate List window. Click on the List button (or press Ctrl+L) to show the list dialog.



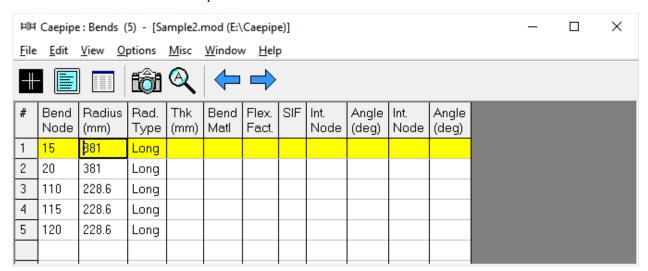
Click on an item of interest to show the list for that item.

A list of all the anchors present in this sample model is shown below:



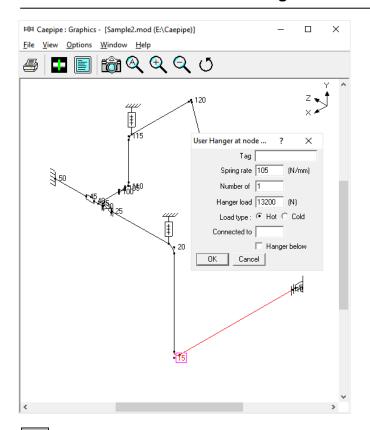
The highlighted item can be edited directly in the List window (in most cases) or in a dialog by pressing Ctrl+E. The items can be deleted by pressing Ctrl+X. The item is also highlighted in the graphics window by flashing and with a box around the node number.

A list of all the bends in the sample model is shown below:

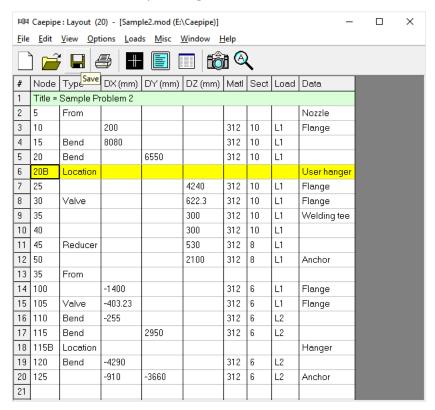


Editing in the Graphics Window

Another useful feature is the ability to edit an item in the graphics window. When an item such as a Hanger is clicked in the graphics window, a dialog box for that item is opened, where it can be modified.

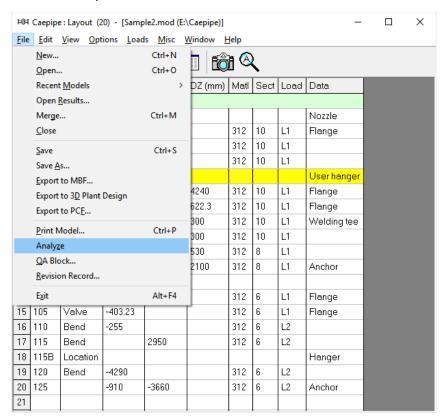


Save the model by clicking on the Save button.

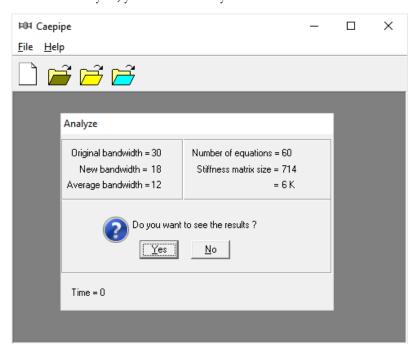


6. Analyze

Click on Analyze under the File menu.

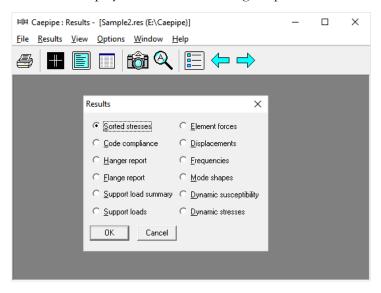


After the analysis, you are asked if you want to see the results. Select Yes.



7. View Results

After finishing the analysis and choosing to see the results or by opening the results file (.res), the results window is displayed. The Results dialog is opened automatically.

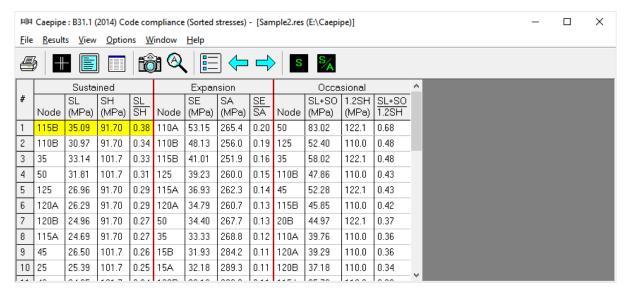


Select an item of interest by clicking on it. When you are viewing the results, use Tab (or Next Result button) to view the next result and Shift+Tab (or Previous Result button) to view the previous result. The Results dialog can be brought up by clicking on the Results button (or press Ctrl+R).

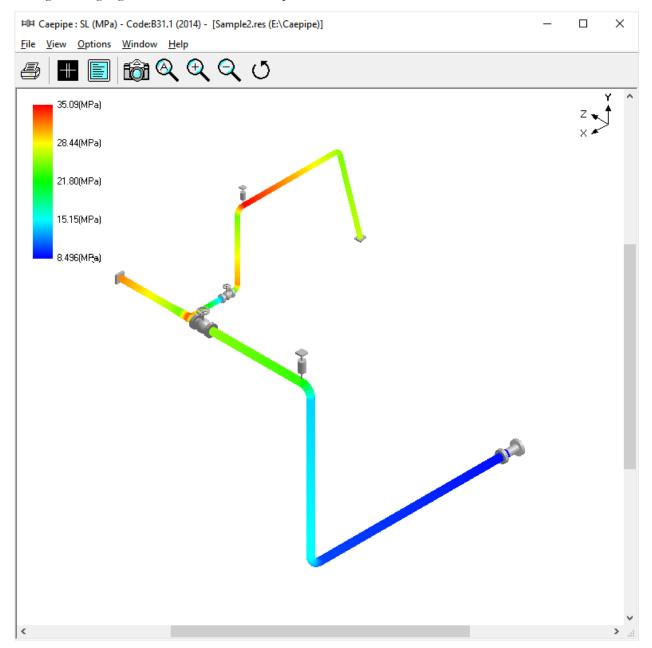
While viewing the results, the model data can also be simultaneously viewed in separate Layout and List windows. These are now "read only" windows, i.e. the model data can not be modified while viewing the results. Some of the results from the sample problem are shown below:

Sorted Stresses

The computed stresses (sustained, expansion and occasional) are sorted in descending order by stress ratios.

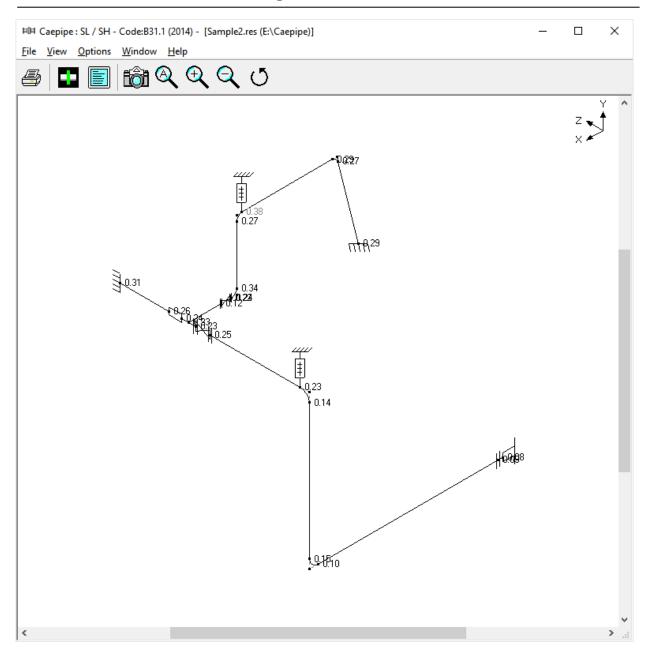


Color coded stresses may be rendered in the graphics window by pressing the Show stresses button (or choose View > Show Stresses). The stresses in the highlighted columns (the bar highlights three columns simultaneously) are displayed in the graphics window. Use the left and right arrow keys to change the highlighted columns or click in a particular column.



The stress ratios may similarly be rendered by using the Show stress ratios button (or choose View > Show Stress Ratios).

Instead of rendering color coded stresses/ratios, the values of stresses/stress ratios may be plotted by using the menu: View > No color coding and pressing the icon S or S/A.

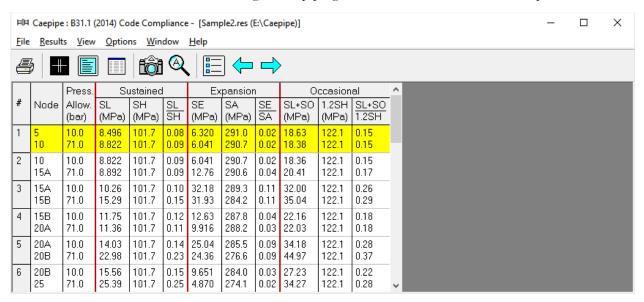


While plotting stresses or stress ratios, thresholds may be specified from the graphics window (choose View > Thresholds). Only the stresses or stress ratios exceeding the thresholds are plotted.



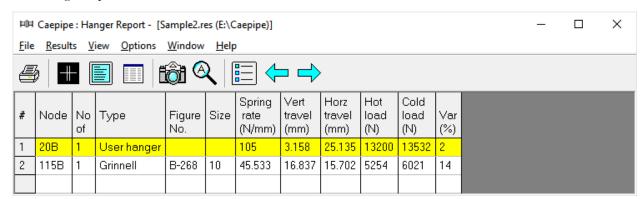
Code compliance

The element stresses calculated according to the piping code are shown under code compliance.



Hanger report

The hanger report is shown below.

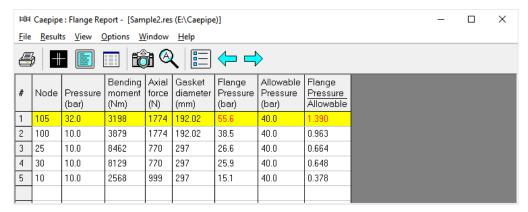


The "No of" field shows the number of hangers required at the indicated location. The Figure No. and Size refer to the manufacturer's catalog. The vertical travel is the vertical deflection at the hanger location for the first operating load case. Similarly, the horizontal travel is the resultant horizontal deflection at the hanger location for the first operating case. The hot load is the hanger load for the operating condition and the cold load is the hanger load at zero deflection.

Variability(%) = (Spring rate \times Hanger travel / Hot load) \times 100

Flange Report

CAEPIPE lists every flange in a model in the flange report. The "Flange Pressure" is an equivalent pressure calculated from the actual pressure in the piping element, the bending moment and the axial force on the flange from the first operating case (W+P1+T1).



The Flange report in the CAEPIPE results window shows the loads at each flange location for the operating case (W+P1+T1).

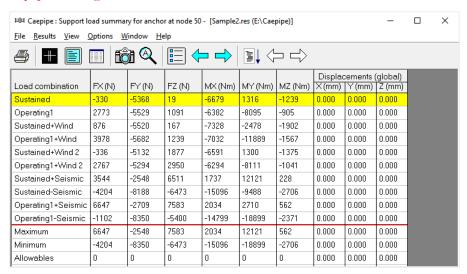
The "equivalent" flange pressure is the sum of three terms from the flange equation as shown in Flange Report section above. The last column shows a ratio of this equivalent flange pressure to a user-input allowable pressure. This ratio is flagged in red when more than 1.0.

Support load summary

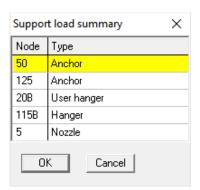
Support load summary for each support is created by considering all the load cases and appropriate combinations and then showing the maximum and minimum loads.

Note: Allowable loads at equipment nozzle can be calculated using the module "Nozzle Allowable loads" available in CAEPIPE through Main Frame > New > Nozzle Allowable Loads.

The allowable loads thus calculated can then be entered as "User Allowables" in CAEPIPE Stress Model through Layout window > Misc. See the CAEPIPE tutorial titled "Tutorial on Qualification of Nozzles to Equipment using CAEPIPE" for more details.

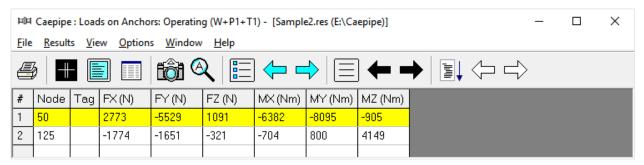


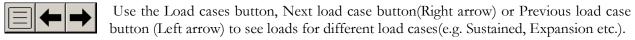
Use the Other supports button (F6), Next support button (Ctrl+Right arrow) or Previous support button (Ctrl+Left arrow) to see loads on other supports (e.g. other anchors, hangers etc.).



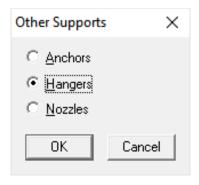
Support loads

Support loads are the loads acting on all the supports of each support type for a specific loading case. The loads on anchors for the Operating case are shown below.

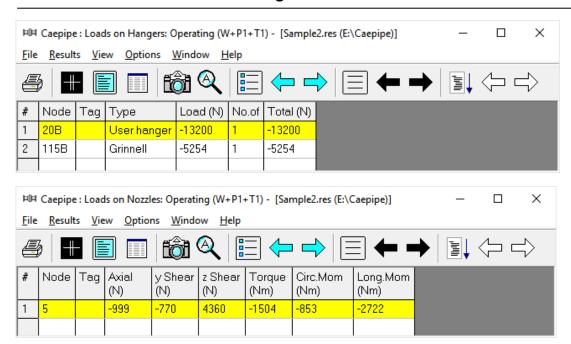




Use the Other supports button (F6), Next support button(Ctrl+Right arrow) or Previous support button (Ctrl+Left arrow) to see loads on supports of different types (e.g. other anchors, hangers etc.).

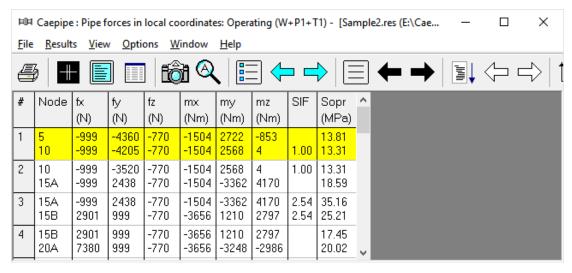


The loads on hangers and nozzle (i.e. the loads acting at the hanger locations imposed by the piping system) for the Operating case are shown below.

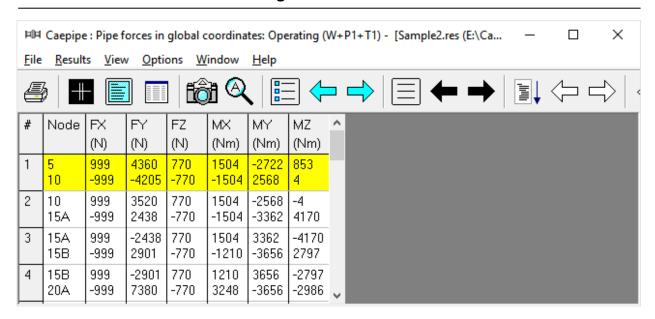


Element Forces

The element forces in local and global coordinates are shown. For pipe (also bend and reducer) element forces in local coordinates, the stress intensification factors (SIFs) and stresses are also shown.



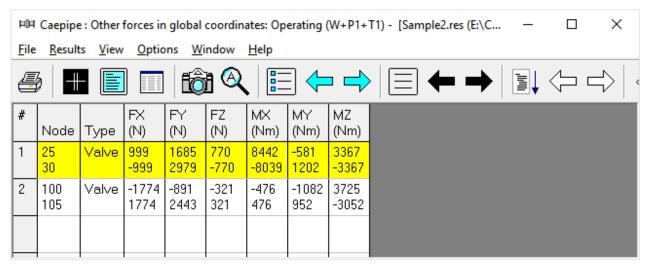
Use the Global forces button (F7) to see the element forces in global coordinates.



Use the Local forces button (F7) to see the element forces in local coordinates again.

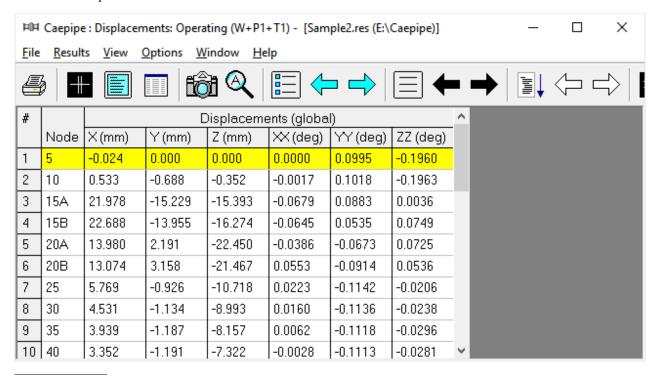
Use the Other forces button (F6), Next force button (Ctrl+Right arrow) or Previous force button (Ctrl+Left arrow) to see other element forces(e.g. valves, bellows etc.).



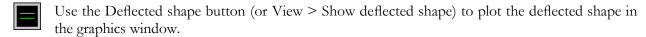


Displacements

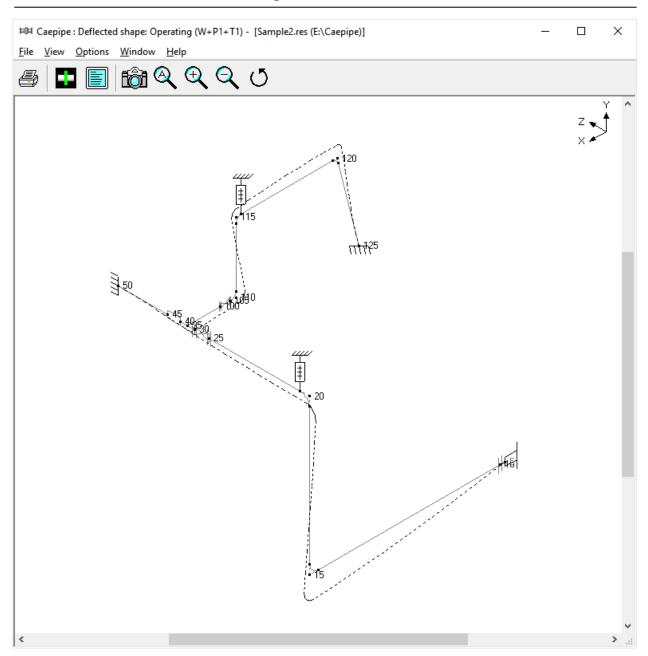
The nodal displacements are shown.



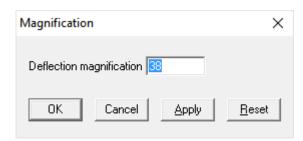
Use the Load cases button, Next load case button (Right arrow) or Previous load case button (Left arrow) to see displacements for different load cases (for example, Sustained, Expansion etc.).



Use the Animated deflected shape button (or View > Show animated deflected shape) to plot the animated deflected shape in the graphics window.



Choose View > Magnification to change the magnification of the deflected shape.

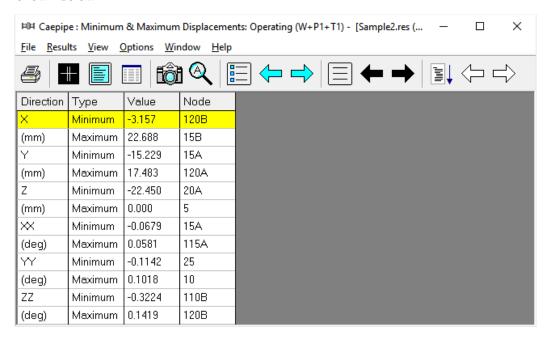


The reset button is used to calculate a default magnification factor which scales the maximum deflection to about 5% of the width of the graphics window.

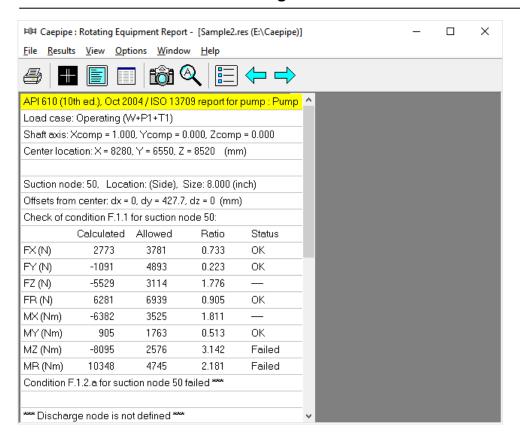
Use the Other displacements button (F6), Next displacement button (Ctrl+Right arrow) or Previous displacement button (Ctrl+Left arrow) to see other displacements (e.g. Min/Max, displacements at hangers, flex joints, limit stops etc.).



The minimum and maximum displacements for each of the directions and the corresponding nodes are shown below.

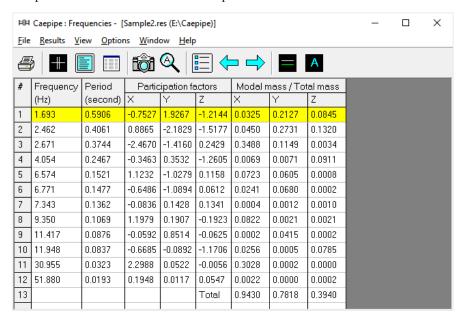


The Pump qualification report (Rotating Equipment report) is shown below.

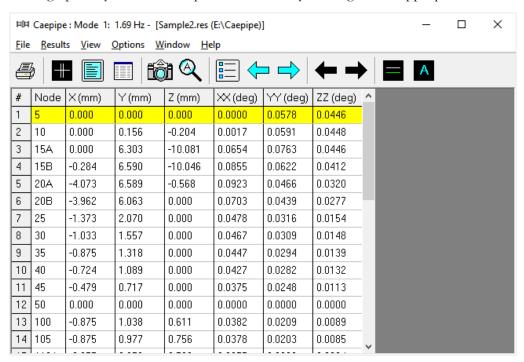


Frequencies

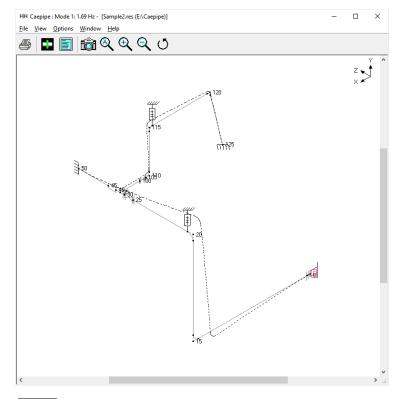
A list of natural frequencies, periods, modal participation factors and modal mass fractions is shown next. You can show each frequency's mode shape graphically or animate it by clicking on Show mode shape or Show animated mode shape button in the toolbar.



Each frequency's mode shape detail is shown in the next window. As in the earlier window, you can show graphically the mode shape or animate it by clicking on the appropriate button.



The graphic window will show the mode shape as thus.

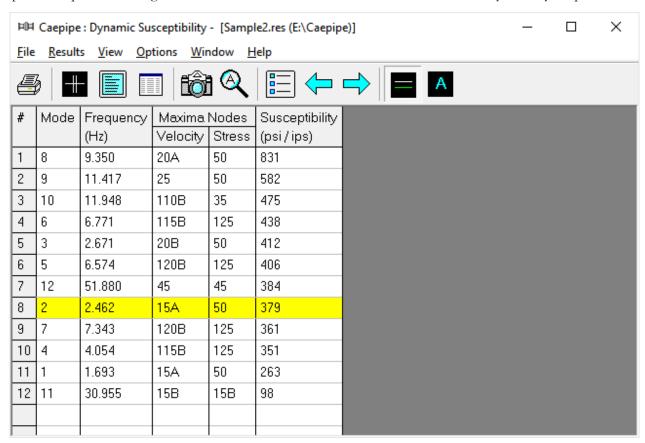


Use the black arrow buttons to cycle through the different Modes.

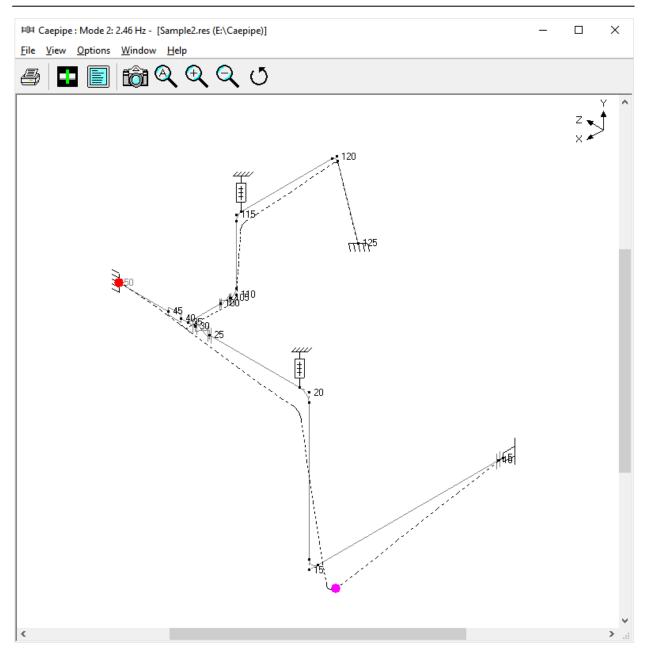
Dynamic Susceptibility

Note: Dynamic Susceptibility is NOT available for Evaluation Version of CAEPIPE. For FULL version of CAEPIPE, this feature can be turned ON by setting an environment variable "HARTLEN" that needs to be declared under My Computer or This PC Icon > Mouse Right Click > Properties > Advanced System Settings > Environmental Variable with its Value set to (YES). Refer to CAEPIPE User's Manual for more details.

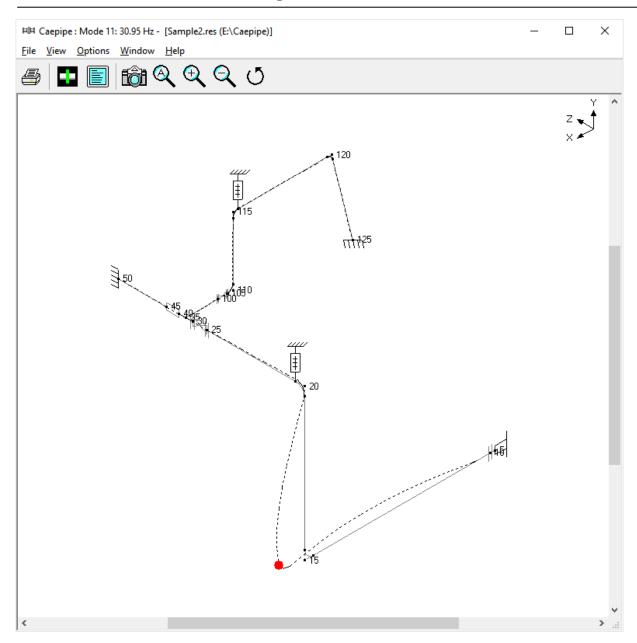
The stress / velocity method, implemented in CAEPIPE as the "Dynamic Susceptibility" feature, provides quantified insights into the stress versus vibration characteristics of the system layout per se.



Pressing the Animated mode shape button (or View > Show animated mode shape) for Mode 2, for example, shows the maximum dynamic bending stress at the Anchor Node 50 (RED dot) and the maximum velocity at the Bend Node 15A (PINK dot).



In case the maximum dynamic bending stress and the maximum velocity occur at the same node for a specific mode, then the RED and PINK dots overlap with each other and only the RED dot is seen for that mode. See the Animated mode shape shown below for mode 11 as an example.

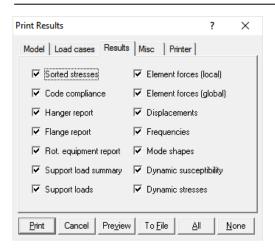


The dynamic susceptibility module *does not apply directly to meeting code or other formal stress analysis requirements.* However, it is an incisive analytical tool to help the designer understand the stress / vibration relationship, assess the situation and to decide how to modify the design if necessary to possibly reduce the susceptibility to vibration. It can be used for design, planning acceptance tests, troubleshooting and correction.

Print

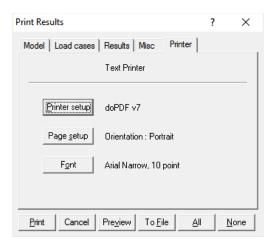


To print results and model data, click on the Print button (or press Ctrl+P). In the Print Results dialog, the items to print can be selected in the property pages.



You can also be print to a text file by using the To File button. A preview of the printed output can be seen by using the Preview button.

The printing options such as choice of printer, margins, portrait or landscape and font can be set on the Printer tab.



The sample problem report is shown next. Observe that for sorted stresses and code compliance, when the stress ratio exceeds 1.00, the stress and the stress ratio are shown in white letters on black background.

This is the end of the tutorial. If you have questions or comments, please email them to: support@sstusa.com

Caepipe		Sample Problem 2		
		Quality Assurance Block		
		Caepipe		
		Version 7.60		
	Client	-		
	Project	£11		
	File Number			
	Report Number			
	Model Name			
	Title	: Sample Problem 2		
	Analyzed	: Mon Sep 12 11:47:34 2016		
	Prepared by	E	Date:	
	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	la constant de la con		
	Checked by	1	Date:	
Version 7.60		Sample2		Sep 12,201

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Mode 10: 11.95 Hz, susceptibility = 1179		28
Mode 6: 6.77 Hz, susceptibility = 815		29
Mode 12: 51.88 Hz, susceptibility = 768		30
Mode 5: 6.57 Hz, susceptibility = 587		30
Mode 2: 2.46 Hz, susceptibility = 445		31
Mode 3: 2.67 Hz, susceptibility = 412		31
Made 7: 7 24 Mar assessmille Street 204		32
Mode 7: 7.34 Hz, susceptibility = 361		33
Mode 11: 30.95 Hz, susceptibility = 249		0.0
Mode 11: 30.95 Hz, susceptibility = 249 Weight & Center of gravity		

													Ana	lvs	is O	ption	s			
0		- 3	Diele		- 004	4 10	0441						7 11112	30		p=0	_			
66	ode		Inclu	g code de axial iberal a	force	in s	ress c		ations											
Te	emper		Numi Numi Then	rence te ber of the ber of the mal = O modulus	nerma nerma perati	l cyc l loai ing -	les = 7 ds = 1 Sustai	000 ned												
Pr	essur		Peak Includ	sure stre pressu de Bour pressur	re fac	tor =	1.00	ends												
Dy	ynamio		Numi Inclu	off frequi ber of m de miss ot use f	nodes ing m	= 20 ass (orrect		lysis											
Mi	isc.			de hang cal direc			s													
													L	ayo	out (20)				
_	_	Туре	_	X (mm	_	(mm	DZ (mm)	Matl	Sec	t Loa	d [Data	1						
-	_	= Samp	le Pro	oblem 2	_				_	_	_	-	_	_	_	4				
-	5	From	1		-				040	-		_	Noza		_	4				
_	10	Dead	-	000	+			_	-	10	L1	-	Flan	ge	_	4				
_	15	Bend	- 8	080	ece	0		-0	312	10	L1	-		_	_	4				
-	20 20B	Bend	-		655	U		-	312	10	L1	-	lees	Sec	-	-				
-	25	Locati	on		+		424	-	312	10	L1	-	User Flan		nge	9				
-	30	Valve	+	_	+		622	_	312	10	L1	_	Flan	_	-	1				
-	35	yaive	+		+		300	3	312	10	L1	-	Velo	_	too	1				
-	40	2.5	+		+		300		312	10	L1	+	iveit	inig	tee	1				
-	45	Redu	er	_	+		530		312	8	L1	+		_	_	+				
_	50	recoun	100		+		210	1	312	8	L1	1	Anch	inr	-	+				
_	35	From			1		-	9	012			1	11.54	101		1				
-	100	T TONI	1.	1400	1			Ť	312	6	L1	1	Flan	ge.	Т	1				
_	105	Valve	-	403.23	+				_	6	L1	-	Flan	_	_	1				
_	110	Bend	-	255	1			- 1	312	6	L2	Ť		3-		1				
-	115	Bend	+		295	0			312	6	L2					1				
8	115B	Locati	on									1	Han	ger	ì	1				
9	120	Bend	-	4290					312	6	L2					1				
0	125		-	910	-366	30	Î		312	6	L2	1	Anch	101	g i	1				
													А	nct	nors	(2)				
loc	de Ta	g KX/k		CY/ky	KZ/ka		(XX/lo		YY/ky		(ZZ/k					ises		I		
		(N/m	-		(N/m	-	Nm/de		Nm/de		Nm/d	eg)	X	Y 2	. X	X Y	/ ZZ		Anchor in Pipe	4
0		Rigio		digid	Rigid		Rigid		tigid		Rigid	_	Ц	1	1	1	1	-	GCS .	4
25	5	Rigio	F	igid	Rigid	F	Rigid	F	tigid	J	Rigid	9	Ц	Berr	nds i	(5)	L	10	3CS	
Ser	vi Ro	adius R	ad I	Thk E	land	Flor	SIF	Int.	An	gle	nt I	An		Dei	ius i	(9)	_	_		
loc		im) T			Mati	Fact		Nod	e (de	gio	Node	(de	(p)							
5	38		ong						1											
0	38		ong			-														
10	_		ong	\neg				20.		1	- 9		\neg							
15	_		ong					c					\exists							
	_		ong	-	-	_		1		_	_		-1							

										Bran	ch SIFs (1	n:			Page
Node	Туре	1								Didin	an on a t	'/			
35		ing tee													
- 10		3								Fla	inges (5)				
Node	Туре	Tv	/eight	Gasket I	Dia Ali	ow Pr	es				a George				
	1,3800	()	g)	(mm)	(ba										
10	Weld	neck 6	9.799	297	40	.0									
25	Weld	neck 6	9.799	297	40	0									
30	Weld	The second second	9.799	and the same of th	40	_									
100	_		-	192.02	40	.0									
105	Weld	neck 2	3.596	192.02	40	.0									
										-	ngers (2)				
Node	Tag	Туре		No Load						ad CNoo	ie				
200		Haras bar	\rightarrow	_	range	+		(N)	_	pe					
20B	-	User ha	\rightarrow	_	-	105	8	132	00 H	ot	-				
15B	ш	Grinnell	- 1	1 25						Ma	zzles (1)				
dada	Te-1	Maar In	leef.	Marris	-	Men	al I	4	10		and the same of	al anda di	natic =	100	
vode		Vess. F Type F		Nozzle D/R Th	k or	Vess VR T	-		L2 (mm)	Modulus (MPa)	X comp	el axis dir	0.77.511	ē.	
5	-	Cyl	-	73.05 9.2		00 9		-		193950	A comp	1 comp	1.000		
,	ш	Cyn	141	3.05 3.2	2/11/10	00 19	.2/1	1500	2100	-	tim	- 785	1.000	(G	
la de	Vess	Dadie	flint I	Circumfer	namilal (lone of	11	Lordina a	I dissell		stiffnesse	S (1)			
voue	Type	Radial (N/mm		(Nm/deg)		KHIC	(Nm/c		l (kml)	1					
5	Cyl	40981	_	4352.04			2737								
-	(),	140001		1002.01		- 23	2101	3.07		Die	np: Pump				
rom	То	OD1	Thk1	OD2	Thk2	Co	ne an	gle			fucers (1)				
From	To	A STATE OF THE PARTY OF THE PAR	1000000				ne an	gle							
40	45	(mm) 273.05	(mm		(mm) 8.178	_	eg)	-							
-	110	270.00	0.27	11210.01	10.170	-		112		Va	alves (2)				
From	To	Weight	Lenc	o Impa	Lincuit	TAdd	i.Wgt		Officiale	of Add.V					
1900		9.516.00		ith I Thick											
		11416031	100000 P	th Thick							-				
75	30	(kg) 459.23	(mm) X	Wgt >					Y (mm) E					
_	30 105	459.23	(mm 622) X 3 3.00											
_	_	459.23	(mm 622) X 3 3.00	Wgt >					Y (mm) E		6)			
100	105	459.23 151.56	(mm 622 403) X 3 3.00 23 3.00	Wgt >					Y (mm) E	OZ (mm)	6)			
100 Node	105	459.23 151.56	(mm 622 403.) X 3 3.00	Wgt >					Y (mm) E	OZ (mm)	6)			
Node	105 X (mr	459.23 151.56 n) Y (r	(mm 622 403	X 3 3.00 23 3.00 Z (mm)	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10	105 X (mr	459.23 151.56 n) Y (r	(mm 622 403 mm)	X 3 3.00 23 3.00 Z (mm)	Wgt >					Y (mm) E	OZ (mm)	6)			
5 10 15A 15	105 X (mr 0 200	459.23 151.56 n) Y (r 0	(mm 622 403.	X 3 3.00 23 3.00 2 (mm) 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15B	X (mr 0 200 7899 8280 8280	459.23 151.56 n) Y (r 0 0	(mm 622 403.	X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15 15B 20A	X (mr 0 200 7899 8280 8280 8280	459.23 151.56 n) Y (n 0 0 0 0 0 381 616	(mm 622 403 mm)	X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15B 20A	X (mr 0 200 7899 8280 8280 8280	459.23 151.56 n) Y (n 0 0 0 0 381 616	(mm 622 403 mm)	X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15B 20A 20 20B	X (mr 0 200 7899 8280 8280 8280 8280 8280	459.23 151.56 m) Y (n 0 0 0 0 0 381 616 655	(mm 622 403 mm)	X 3 3.00 23 3.00 Z (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 55 110 115A 115B 20A 20 20B	X (mr 0 200 7899 8280 8280 8280 8280 8280 8280	459.23 151.56 n) Y (n 0 0 0 0 381 616 655 655	(mm) 403mm) 3	X 3 3.00 23 3.00 Z (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15 15B 20A 20 20B 225	X (mr 0 200 7899 8280 8280 8280 8280 8280 8280 8280	459.23 151.56 n) Y (n 0 0 0 0 381 616 655 655	(mm) 403mm) 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	X X 3 3.00 Z (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 110 115A 115 115B 20A 20 20B 225 330	X (mr 0 200 7899 8280 8280 8280 8280 8280 8280 8280 8	459.23 151.56 n) Y (n 0 0 0 0 0 381 616 655 655 655	(mm) 403.	X X 3 3.00 Z (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15 15B 20A 20 20B 25 30	X (mr 0 200 7899 8280 8280 8280 8280 8280 8280 8280 8	459.23 151.56 n) Y (n 0 0 0 0 0 381 616 655 655 655 655	(mm) 2 403.	X X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15 15B 20A 20 20B 25 30 35	X (mr 0 200 7899 8280 8280 8280 8280 8280 8280 8280 8	459.23 151.56 n) Y (n 0 0 0 0 0 381 616 655 655 655 655	(mmm)	X X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15B 20A 20 20B 25 30 335 40	X (mir 0 200 7899 8280 8280 8280 8280 8280 8280 8280 8	459.23 151.56 n) Y (n 0 0 0 0 0 381 616 655 655 655 655 655	99 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	X X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			
Node 5 10 15A 15 15B 20A 20 20B 25 30 35	X (mr 0 200 7899 8280 8280 8280 8280 8280 8280 8280 8	459.23 151.56 n) Y (n 0 0 0 0 381 616 655 655 655 655 655	(mmm) 622 403 100	X X 3 3.00 23 3.00 2 (mm) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wgt >					Y (mm) E	OZ (mm)	6)			

Caepip	pe								Sample P	roblem 2	Ş	Page
			911						Coordina	ites (26)		
lode	X (mn	n) Y	(mm)	Z (mm)								
10A	6450.	37 6	550	5162.3								
10	6221.	77 6	550	5162.3								
10B	6221.	77 6	778.6	5162.3								
115A	6221.	77 9	271.4	5162.3								
115	6221.	77 9	500	5162.3								
115B	5993.	17 9	500	5162.3								
120A	2110.	49 9	500	5162.3								
-	1931.	enterior de maior	-	5162.3								
-	NAME AND ADDRESS OF THE PARTY O	_	326.56	AND DESCRIPTION OF								
_	1021.	_		5162.3								
1,000	276.11		e.e. 1	0.749670				Pine r	naterial 31	2: A312	TP31	6
Sancit	v = 80	27 Ib	a/m3) A	hr = 0.30	O Join	t factor	= 1.00, Ty		natorial o	E. POTE	11 011	**
_	-	_		1,000,000		LIGIGION	= 1.00, Ty	pe-no				
Temp (C)	(MPa		Vipha mm/mm/	Allow C) (MPa								
_	-	_	4.90E-6	137.9	_							
37.78	-	-	5.46E-6	137.9	_							
93.33	-	-	6.02E-6	119.3								
-	-		nintranintrane	_	_							
148.9	-	_	6.56E-6	107.6								
204,4	_	_	7.10E-6	98.60								
260	_	_	7.46E-6	91.70	_							
15.6	_	_	7.82E-6	86.87	_							
343.3	-	_	7.91E-6	84.81	_							
371.1	-		8.00E-6	83.43	_							
398.9	-	-	8.09E-6	82.05	_							
426.7	_	_	8.18E-6	81.36								
454,4	-	_	8.27E-6	79.98	_							
482.2	1620	_	8.36E-6	79.29	_							
510	-	_	8.45E-6	78.60	_							
537.8	1572	-	8.54E-6	77.91								
565.6	-	-	8.81E-6	77.22	_							
593.3		_	8.72E-6	76.53	3							
621.1	-	-	8.90E-6	67.57	7							
648.9	1461	69 1	9.08E-6	51.02	2							
	200								Pipe Sec	tions (3)		
Name	Nom	Sch	OD	Thk	Cor.Al		Ins.Dens	Ins.Thk	Lin.Dens	Lin.Thk	Soil	
	Dia		(mm)	(mm)	(mm)	(%)	(kg/m3)	(mm)	(kg/m3)	(mm)		
3	6"		168.27				176.2	65				
3	8"			8.1788			176.2	65				
0	10"	STD	273.05	9.271			176.2	65				
									Los	ids		
Static:	seismi	c load	1: X = 0.	30, Y = 0	.20, Z :	0.30 (g's)					
							of Squares	i				
									Wind	load 1		
	factor											
				1.000, Y	comp =	0.000,	Z comp =	0.000				
Elevat	ion I	Velo	city									
m)		(kmh										
)		100										
20		100	\neg									
									Wind	oad 2		
Shano	factor	= 0	60									
Nind o	direction	n: X	comp = (0.000. Y	comp =	0.000	Z comp =	1,000				
-01050				- T. F. F. S. C.				COLUMN TO				
/arcin	7.00								Sam	-1-0		Sen 12 20

aepip	_	Valacit	v							Sample	
nevat m)		Velocit (kmh)	4								
-	-	100	\neg								
0	\rightarrow	100	\neg								
	- 1		- 10							Pipe I	oads (2)
lame	T1	P1	Specifi	c Add.	Wgt. V	Vind					
	(C)	(bar)	gravity	1000000	- W-	.oad					
1	185	10.0	0.1		- 1	1					
2	260	32.0	0,1		- 1						
					- 757			B31.1 ((2014) C	ode cor	npliance
	0.78	ained	1			nsion	-			sional	
	SL (MPa)	SH (MPa	SL	Node	SE /MPal	SA (MPa)	SE SA	Node	(MPa)		SL+SO 1.2SH
-	35.09	-	in the same		53.15		0.20	50	83.02	122.1	0.68
-	30.97	_	-	110B	_	-	0.19	125	52.40		0.48
_	33.14	-	_	115B		-	0.16	35	58.02	122.1	0.48
-	31.81	-	0.31	125	39.23	_	0.15		47.86	-	0.43
-	26.96		-	-	36.93	-	0.14		52.28		0.43
20A	26.29	91.70	-	120A	34.79	260.7	0.13	115B	45.85	110.0	0.42
20B	24.96	91.70	0.27	50	34.40	267.7	0.13	20B	44.97	122.1	0.37
15A	24.69	91.70	0.27	35	33.33	268.8	0.12	THE REAL PROPERTY.	39.76	110.0	0.36
5	26.50	101,7	0.26	15B	31.93	284.2	0.11	120A	39.29	110.0	0.36
5	25.39	101.7	0.25	15A	32,18	-	0.11		37.18	110.0	0.34
_	24.65	101.7		120B	29.10	-	0.11	115A	35.78	110.0	0.33
_	21.59		0.24	105	24.73	_	0.09	15B	35.04	122.1	0.29
-	23.82	-	-	20B	24.36	-	0.09	105	31.30	-	0.28
-	22.98	and the same of	-	20A	25.04	THE REAL PROPERTY.	0,09	25	34.27	122.1	0.28
	20.09	_	_	100			-	20A	34.18	122.1	0.28
\rightarrow	15.29	-	_	45	21.86	_	1.00	40	33.84	122.1	0.28
-	14.03	101.7	-	40 5	6.189		0.02	30 15A	32.81	122.1	0.27
-	10.26	-	0.12		6.041	290.7	0.02	100	24.27	122.1	0.20
-	8.822	101.7	-	-	5.582	-	0.02	-	18.63	122.1	0.15
\rightarrow	8.496		0.08	10.7	4.870	-	0.02		18.38	-	0.15
		XII	100	177						-	Code Cor
T	Press.		Sustaine	ed	E	xpansio	n		Occasio		T
ode	Allow.	SL	SH	SL	SE	SA	SE	SL+S		SL+S	
	(bar)		(MPa			(MPa)		(MPa		-	Н
	10.0 71.0			0.08		291.0 290.7				0.15	
-	10.0		_			290.7				0.15	-
	71.0					290.6					
_	10.0		101.7		32.18					-	
200	71.0	15.29	101.7	0.15	31.93	284.2	0.11	35.04	122.1	0.29	
0.00	10.0					287.8				0.18	
-	71.0	_	_	_	_	288.2	_	_		0.18	-
200	10.0 71.0					285.5 276.6				0.28	
-	10.0	15.56	_	_	9.651	-	-	27.23	_	-	-
N-02	71.0					274.1				0.28	
_	10.0	_	_	_		_	_	32.81	_	0.27	7
5	71.0		101.7	7 0.33	14.89	266.4	0.06	50.26	122.1	0.41	
500	10.0	32.98		0.32						0.35	-
-	71.0	COLUMN TWO	-	OTHER DESIGNATION OF THE PERSON NAMED IN	National Control	280.6	THE OWNER WHEN	-	-	0.21	4
0	10.0	24.65			6.189	274.9				0.28	
5					121.00	400000	19.00	104.20	1166.	10.43	- 4.

Caepip	pe								S	ample P	roblem 2	Pag
-									B31.1 (2	2014) Co	de Compliance	
20.30	Press.		ustaine	_		xpan			ocasion			
lode	Allow.	SL	SH	SL	SE	SA	SE		1.2SH	SL+SC		
5	(bar) 10.0	(MPa) 19.90			_	_	a) SA	(MPa) 4 37.47	(MPa)	1.2SH		
. 300	78.3							3 83.02	122.1			
-	10.0	30.78		-	_	_	_	2 58.02	122.1		Í	
_	89.0	12.39	101.7	0.12	23.0	2 287	.1 0.0	8 24.27	122.1	0.20		
	32.0	20.09			24.73			9 31.30	110.0			
10A	and the latest designation of the latest des	20.59						9 31.78	110.0			
	32.0 80.2	21.59 30.97						0 39.76 9 47.86	110.0			
	32.0							9 37.15	110.0		·	
	80.2							7 29.82	110.0			
_	32.0	24.69	91.70	0.27	36.93	3 262	.3 0.1	4 35.78	110.0			
$\overline{}$	80.2							6 45.85	110.0			
	32.0	28.91						7 35.57	110.0			
$\overline{}$	80.2 32.0			-	_	_	_	6 31.58 3 39.29	110.0	_		
	80.2	26.29 24.96						1 37.18	110.0			
20B		22.61	_	_	13.50		_	5 30.19	110.0		Í	
	80.2							5 52.40	110.0			
									į.	Hanger	Report	
74					S	pring	Vert	Horz	Hot	Cold		
	No Ty	pe	No	gure 5		ate Jimm)	(mm)	travel (mm)	load (N)	load (N)	Var (%)	
_	_	ser hang	_	+	_	05	3.158					
-	_	innel	_	268	-	5.533	16.83	_		6021	14	
- 100	100									Flange	report	
		Ber	iding A	Axial	Gaske	t Fl	ange	Allowable	Flang	е		
1000004		1000				CONTRACTOR		Pressure				
$\overline{}$	(bar)	(Nn	_		(mm)	(b		(bar)	Allow			
_	32.0 10.0	319	_	_	192.02	_		40.0	0.963			
_	10.0	846	-	_	297	26		40.0	0.664	_		
-	10.0	812	_	-	297	25		40.0	0.648	_		
	10.0	256	_	_	297	15		40.0	0.378			
0.224	n 7.60									Sam		Sep 12,20

Caepipe Sample Problem 2 Page 6 API 610 (11th ed.), Sep 2010 / ISO 13709 report for pump : Pump Load case: Operating (W+P1+T1) Shaft axis: Xcomp = 1.000, Ycomp = 0.000, Zcomp = 0.000 Center location: X = 8280, Y = 6550, Z = 8520 (mm) Suction node: 50, Location: (Side), Size: 8.000 (inch) Offsets from center: dx = 0, dy = 427.7, dz = 0 (mm) Check of condition F.1.1 for suction node 50; Calculated Allowed Status 2773 3781 -1091 4893 FX (N) 0.733 FY (N) FZ (N) -1091 0.223 ОК 3114 1.776 -5529 OK FR (N) 6281 6939 0.905 MX (Nm) 3525 -6382 1.811 MY (Nm) 905 1763 0.513 OK MZ (Nm) -8095 2576 3.142 Failed MR (Nm) 10348 4745 2.181 Failed Condition F.1.2.a for suction node 50 failed *** *** Discharge node is not defined ***

Caepipe					Sa	mple Prob	lem 2			Pa
			40	Suppo	ort load su	mmary for	anchor a	at node 5	0	
			1	T			Displa	ements	(global)	
Load combination	FX (N)	FY (N)	FZ (N)	MX (Nm)		MZ (Nm)	X (mm)	Y (mm)	Z (mm)	
Sustained	-330	-5368	19	-6679	1316	-1239	0.000	0.000	0.000	
Operating1	2773	-5529	1091	-6382	-8095	-905	0.000	0.000	0.000	
Sustained+Wind	876	-5520	167	-7328	-2478	-1902	0.000	0.000	0.000	
Operating1+Wind	3978	-5682	1239	-7032	-11889	-1567	0.000	0.000	0.000	
Sustained+Wind 2	-336	-5132	1877	-6591	1300	-1375	0.000	0.000	0.000	
Operating1+Wind 2	2767	-5294	2950	-6294	-8111	-1041	0.000	0.000	0.000	
Sustained+Seismic	3544	-2548	6511	1737	12121	228	0.000	0.000	0.000	
Sustained-Seismic	-4204	-8188	-6473	-15096	-9488	-2706	0,000	0.000	0.000	
Operating1+Seismic	6647	-2709	7583	2034	2710	562	0.000	0.000	0.000	
Operating1-Seismic	-1102	-8350	-5400	-14799	-18899	-2371	0.000	0.000	0.000	
Maximum	6647	-2548	7583	2034	12121	562	0.000	0.000	0.000	
Minimum	-4204	-8350	-6473	-15096	-18899	-2706	0.000	0.000	0.000	
Allowables	0	0	0	0	0	0	0.000	0.000	0.000	
				Suppo	rt load sun	nmary for	anchor a	t node 1	25	
N 27 SW/65	200000	10000	100000	· ·		200000	Control of the control	ements	10	
Load combination	FX (N)	FY (N)	FZ (N)		MY (Nm)		-	-	-	
Sustained	230	-1727	28	45	-39	-1179	0.000	0.000	0.000	
Operating1	-1774	-1651	-321	-704	800	4149	0.000	0.000	0.000	
Sustained+Wind	821	-1714	-64	-183	124	-2172	0.000	0.000	0.000	
Operating1+Wind	-1182	-1637	-412	-932	963	3157	0.000	0.000	0.000	
Sustained+Wind 2	240	-1723	698	1797	-463	-1199	0.000	0.000	0.000	
Operating1+Wind 2	-1764	-1646	350	1049	376	4129	0.000	0.000	0.000	
Sustained+Seismic	1504	-1105	826	2162	694	1524	0.000	0.000	0.000	
Sustained-Seismic	-1045	-2349	-771	-2073	-773	-3882	0.000	0.000	0.000	
Operating1+Seismic	-499	-1029	477	1414	1533	6852	0.000	0.000	0.000	
Operating1-Seismic	-3048	-2272	-1120	-2822	66	1447	0.000	0.000	0.000	
Maximum	1504	-1029	826	2162	1533	6852	0.000	0.000	0.000	
Minimum	-3048	-2349	-1120	-2822	-773	-3882	0,000	0.000	0.000	
Allowables	0	0	0	0	0	0	0.000	0.000	0.000	
				Suppo	rt load sun	nmary for h	nanger a	t node 2	08	
			cements (
Load combination	_	THE REAL PROPERTY.	Y (mm)	CONTRACTOR OF STREET						
Sustained	-13283	-2.816	-	0.000						
Operating1	-13200	13.074	3.158	-21.467						
Sustained+Wind	-13442	4.505		0.000						
Operating1+Wind	-13359	20.396	1.647	-21.467						
Sustained+Wind 2	-13490	-2.030	-	800.0						
Operating1+Wind 2	-13407	13.861		-21.459						
Sustained+Seismic	-11735	14.472	17.113							
Sustained-Seismic	-14831	-	-12.377	THE RESERVE THE PERSON NAMED IN						
Operating1+Seismic			17.902							
Operating1-Seismic	-14748	-4.214	-11.587							
Maximum	-11652	30,363	17.902							
Minimum	-14831	-20.105	-12.377	-21.491						
		0.0000000000000000000000000000000000000		Suppor	t load sum	mary for h	anger at	node 11	5B	
		Displac	ements (g	(ladol)		200	1780			
Load combination		_	Y (mm) 2							
Sustained	-5949	_		0.166						
Operating1	-5254	13.734		7.611						
Sustained+Wind	-5948	2.981	-	1.166						
Operating1+Wind	-5252	15.260	16.870 -	8.944						

	pe								Sample	Problem 2					Page
				you 43				Support	load summar	y for hanger at nod	e 115B				
						ments									
	combir	100000	-			Y (mm)	_								
-	ined+V		-5948	1,4	-	1,591	4.848	-							
_	_	Wind 2	-	_	_	16.866	-2.93								
		Seismic	-5757	5.5	_	5.785	7.278								
		eismic	-6142	-2.6	_	2.662	-6.94	_							
-income	-	Seismic	-	-	-	21.061	-0.50	-							
männen	_	Seismic	-5446	9.5	-	-	-14.7								
Maxim			-5062	_	_		7.278	-							
Minim	um	_	-6142	-2.6	180	2.662	-14,7	23							
							_	0	and found account	and the annual state	4. 5				
			lac acres				1 2		_	ary for nozzle at no					
oad (combin	nation	Radial	(P)	5000000	ar (VL)		ear (VC	A DESCRIPTION OF THE PARTY OF T	E. Proposition of the Control of the	Long.Mom (ML)		ements		
			(N)	_	(N)		(N)		(Nm)	(Nm)		announce of the last of the la	-	Z (mm)	
Sustai	-	_	100		-47	8	366		319	-214 -853	-392	0.000	0.000	0.000	
Opera		Allord	-999 944	-	-770 -103	U .	436 345		-1504	-853	-2722 -208	-0.024	0.000	0.000	
	ined+V		-155	<u> </u>	-103	9	415			-215	0.000	0.023	0.000	0.000	
-	ting1+		-155 96			8	-		-1818	-	-2538	-0.004	0.000	0.000	
	ined+V		-1003	-	174		370 439		-1440 -3263	-288 -927	1547 -783	0.000	0.000	0.000	
		Wind 2 Seismic	3956	-	174	(6)	479		3227	326	3285	-0.024 0.097	0.000	0.000	
_	_	eismic	-3755	_	-181	_	253		-2588	-753	-4068	-	-	-	
				-	994		549			-313	954	-0.092	0.000	0.000	
	_	Seismic Seismic		_	-2534		322		1404 -4411	-1392	-6399	-0.118	0.000	0.000	
Maxim	-	Seismic	3956	-8	1717		549		3227	326	3285			0.000	
Minim		-	-4855	-	-2534		253	-	-4411	-1392	-6399	-0.118	0.000	0.000	
Allowa	-	-	0	-	0	*:	0	*	0	0	0	0.000	0.000	0.000	
HUNC	mes		10.:		10		10	Le	1-	rs: Sustained (W+I	17	0.000	0.000	0.000	
						Tanza.	()			is. Sustained (WF)	7.				
dad.	T 1	TW MIN	EV AB	100											
STATE OF THE PARTY	Tag		FY (N)	_	(N)	-	-	-	MZ (Nm)						
50		-330	-5368	19		-6679	1	316	-1239						
50			THE REAL PROPERTY.	_		-	1	316 39	-1239 -1179	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ph.				
50 125		-330 230	-5368 -1727	19 28		-6679 45	1	316 39	-1239 -1179	ers: Sustained (W+	P)				
50 125 Node	Tag	-330 230 Type	-5368 -1727 Los	19 28 ad (N)	No.ol	-6679 45 Total	(N)	316 39	-1239 -1179	ers: Sustained (W+I	P)				
50 125 Node 20B	Tag	-330 230 Type User har	-5368 -1727 Loanger -13	19 28 ad (N) 283	No.of	-6679 45 Total -1328	(N) 3	316 39	-1239 -1179	ers: Sustained (W+i	P)				
50 125 Node 20B	Tag	-330 230 Type	-5368 -1727 Loanger -13	19 28 ad (N)	No.ol	-6679 45 Total	(N) 3	316 39 Lo	-1239 -1179 ads on Hange						
50 125 Node 20B 115B	Tag	-330 230 Type User har Grinnell	-5368 -1727 Loanger -13	19 28 ad (N) 283	No.of	-6679 45 Total -1328	(N) 3	316 39 Lo	-1239 -1179 ads on Hange	ers: Sustained (W+i					
50 125 Node 20B 115B	Tag (-330 230 Type User har Grinnell	-5368 -1727 Los nger -13 -59	19 28 ad (N) 283 49 z Sh	No.of	-6679 45 Total -1328 -5949	(N)	316 39 Lo	-1239 -1179 ads on Hange bads on Nozzli						
50 125 Node 20B 115B	Tag (-330 230 Type User har Grinnell Axial (N)	-5368 -1727 Loanger -13 -59 y Shear (N)	19 28 ad (N) 283 49 z Sh	No.of	-6679 45 Total -1328 -5949 orque	(N) 3 Circ.N	316 39 Lo	-1239 -1179 lads on Hange lads on Nozzli ong Mom						
50 125 Node 20B 115B	Tag (-330 230 Type User har Grinnell	-5368 -1727 Los nger -13 -59	19 28 ad (N) 283 49 z Sh	No.of	-6679 45 Total -1328 -5949 orque	(N) 3 Circ.N (Nm)	316 39 Lo Lo Hom Lo (N	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 125 Node 20B 115B Node	Tag (330 230 Type User har Grinnell Axial (N)	-5368 -1727 Loanger -13 -59 y Shear (N) -47	19 28 ad (N) 283 49 z Sh- (N) 3666	No.of	-6679 45 Total -1328 -5949 orque (m)	(N) 3 Circ.N (Nm) -214	316 39 Lo Lo Lo (N -3	-1239 -1179 lads on Hange lads on Nozzi long, Mom		p)				
50 125 Node 20B 115B Node	Tag /	330 230 Type User har Grinnell Axial (N)	-5368 -1727 Los nger -13 -59 y Shear (N) -47	19 28 ad (N) 283 49 z Sh- (N) 3666	No.of	-6679 45 Total -1328 -5949 orque (m)	(N) 3 Circ.N (Nm)	Lo Lo Lo Lo Lo Nipe force SL	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 125 Node 20B 115B Node	Tag /	330 230 Type User har Grinnell Axial (N) 100	-5368 -1727 Loanger -13 -59 y Shear (N) -47	19 28 ad (N) 283 49 z Sh (N) 3666	No.of 1 1 1 ear Ti (N) 3	-6679 45 Total -1328 -5949 orque im) 19	(N) 3 Circ.N (Nm) -214	Lo Lo Lo Lo Lo Nom Lo (N -3	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
Node 125 Node 115B Node	Tag fx (N)	Type User har Grinnell Axial (N) 100 fy (N) -3666	-5368 -1727 Los nger -13 -59 y Shear (N) -47	283 ad (N) 2283 449 z Sh (N) 3666	No.of 1 1 1 1 my (Nm) 392	-6679 45 Total -1328 -5949 orque im) 19	(N) 3 3 Circ.N (Nm) -214 F	316 39 Lo	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
Node 20B 115B Node 5	Tag / (1) Tag / (1) Tag / (1) 100 100	330 230 Type User har Grinnell Axial (N) 100 fy (N) -3666 -3511	-5368 -1727 Loanger -13 -59 y Shear (N) -47 (N) (-47 3 -47 3	19 28 ad (N) 283 449 z Shi (N) 3666 Nmx Nm) 319 319	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 Total -1328 -5949 orque (m) 19 mz (Nm) -214 504	(N) 3 Circ.N (Nm) -214 F	316 39 Lo flom L4 (N -3 ipe forc SL (MPa) 8.496 8.822	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
Node 20B 115B Node 5 Node	Tag / (4) Tag / (4) Tag / (10) Tag / (10)	330 230 Type User har Grinnell Axial (N) 100 fy (N) -3666 -3511 -2827	-5368 -1727 Loanger -13 -59 y Shear (N) -47 fz r (N) (19 28 ad (N) 2283 449 z Sh(N) 3666 Nmx Nm) 319 319 319	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 Total -1328 -5949 orque (Nm) 19 mz (Nm) -214 504	(N) 3 Circ.N (Nm) -214 F	316 39 Lo flom L(N) -3 ipe forc SL (MPa) 8.496 8.822 8.822	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 1125 Node 20B 115B Node 5 Node 10 10	Tag / (N) 100 100 100	330 230 Type User har Grinnell Axial (N) 100 fy (N) -3666 -3511 -2827 3132	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47	283 add (N) 2283 449 z Shi (N) 3666 Nmx Nm) 319 319 319	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 -1328 -5949 -5949 mz (Nm) -214 504 -670	(N) 3 Circ.N (Nm) -214 F 1.00	316 39 Lo forn Lo (N -3 2)pe forc SL (MPa) 8.496 8.822 8.822 8.822 8.892	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
Node 20B 115B Node 5 Node 5 10 10 15A	Tag / (4) Tag / (4) Tag / (10) Tag / (10)	330 230 Type User har Grinnell Axial (N) 100 fy (N) -3666 -3511 -2827 3132	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47 -47	283 add (N) 2283 449 z Shi (N) 3666 mx Nm) 319 319 319	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 Total -1328 -5949 orque (Nm) 19 mz (Nm) -214 504	(N) 3 Circ.N (Nm) -214 SIF 1.00	316 39 Lo Iom Lo (N -3 *pe forc SL (MPa) 8.496 8.822 8.822 8.892	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
Node 20B 115B Node 5 Node 5 10 10 15A 15B	Tag / (N) 100 100 100 100	330 230 Type User har Grinnell Axial (N) 100 fy (N) -3666 -3511 -2827 3132 -100	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47 -47 -47 -47 -47	283 add (N) 2283 449 z Shi (N) 3666 mx Nm) 319 319 319 319	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 -1328 -5949 -5949 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7	(N) 3 Circ.N (Nm) -214 F 1.00 1.00	316 39 Lo Iom Lo (N -3 *pe forc SL (MPa) 8.496 8.822 8.822 8.892	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 125 Node 20B 115B Node 5 Node 5 10 10 15A 15B 15B	Tag / (N) 100 100 100 100 3595	330 230 Type User har Grinnell Axial (N) 100 fy (N) -3666 -3511 -2827 3132 -100 -100	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47 -47 -47 -47 -47	28 and (N) 283 49 2 Sh-(N) 3666 mx Nm) 319 319 319 319 319 319	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 -1328 -5949 -5949 -704 -704 -704 -704 -704 -704 -704 -704	(N) 3 Circ.N (Nm) -214 F 1.00 1.00	316 39 Lo Iom Lo (N -3 3pe forc SL (MPa) 8.496 8.822 8.822 8.822 10.26 15.29	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 125 125 Node 20B 115B 115B Node 5 10 10 15A 15A 15B 15B 20A	Tag / (N) 100 100 100 100 3595 3595	7ype User har Grinnell (N) 100 -3666 -3511 -2827 3132 -100 -100 -100	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47 -47 -47 -47 -47	19 28 28 349 2 Shirth (N) 3666 319 3	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 -1328 -5949 -5949 -7214 -504 -670 -670 -1889 -1310	(N) 3 Circ.N (Nm) -214 F 1.00 1.00	316 39 Lo Iom Lo (N -3 2)pe force SL (MPa) 8.496 8.822 8.822 8.822 10.26 15.29 11.75 11.36	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 125 Node 20B 115B Node 5 10 10 15A 15A 15B 15B 15B 20A 20B	Tag () fx (N) 100 100 100 100 3595 3595 8074	7ype User har Grinnell (N) 100 -3666 -3511 -2827 3132 -100 -100 -100	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47 -47 -47 -47 -47	19 28 28 349 28 3666 36	No.ol 1 1 1	-6679 45 -1328 -5949 -5949 -7214 -504 -670 -670 -1889 -1310 -608 -1310 -608 -3814	(N) 3 3 Circ.N (Nm) -214 F 1.00 1.00 2.54 2.54	316 39 Lo lom Lo (MPa) 8.496 8.822 8.822 8.822 10.26 15.29 11.75 11.36 14.03 22.98	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				
50 125 Node 20B 115B Node 5 Node 5 10 10 15A 15B 15B 15B 15B 20A	Tag / (K) Tag /	7ype User har Grinnell (N) 100 -3666 -3511 -2827 3132 -100 -100 -47 -8537	-5368 -1727 Loanger -13 -59 y Shear (N) -47 -47 -47 -47 -47 -47 -47 -47 -47 -47	19 28 28 349 2 Shripting 19 28 3 3 3 3 3 3 3 3 3	No.ol 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6679 45 -1328 -5949 -5949 -7214 -504 -670 -670 -1889 -1310 -608	(N) 3 3 Circ.N (Nm) -214 F 1.00 1.00 2.54 2.54	316 39 Lo lom Lo (MPa) 8.496 8.822 8.822 8.822 10.26 15.29 11.75 11.36 14.03 22.98 15.56	-1239 -1179 lads on Hange lads on Nozzi long, Mom	as: Sustained (W+f	p)				

Caepi	μe								Sample Problem 2 Pa
- 50				, ,			_		local coordinates: Sustained (W+P)
Node		fy (N)	fz (N)	mx (Nm)	my (Nm)	mz (Nm)	SIF	SL (MPa)	
30	(N) -47	4274		-1272	-482	7954	1.00	23.82	
35	-47	4506	-100	-1272	-512	6637		33.14	
35	-19	3613	-330	1239	-350	6612		32.98	
40	-19	3845	-330	1239	-449	5494		18.89	
40	-19	3845	-330	1239	-449	5494		24.65	
45 45	-19	4196	-330	1239	-624	3363	2.00	26.50 19.90	
50	-19 -19	4196 5368	-330 -330	1239 1239	-624 -1316	3363 -6679		31.81	
35	230	894	28	25	-162	2511	2.49	30.78	
	230	1432		25	-123	883	Sec. 201	12.39	
105	230	3446	28	25	-112	-100	1.00	20.09	
-	230	3456	28	25	-111	-191		20.59	
	230	3456	28	25	-111	-191		21.59	
110B 110B	3594	-230 230	28 -28	-105 -105	-19 19	-940 940	2.17	30.97 26.72	
115A		230	-28	-105	-50	368		22.96	
	4551	230	-28	-105	-50	368	2.17	24.69	
115B	230	-4689		-56	98	1376	2.17	35.09	
115B	0.72330	-1260		-56	-98	-1376	10 0	28.91	
120A		231	28	-56	9	623	0.47	23.48	
	230 -282	-231 -307	-28 -28	-56 -27	-9 47	-623 -521	2.17	26.29 24.96	
_	-282	307	28	-27	-47	521	2.11	22.61	
125	-1621	640	28	-27	53	-1179		26.96	
							0	ther for	n local coordinates: Sustained (W+P)
-		fx	fy	fz	mx	my	mz		
Node	_	(N)	(N)	(N)	-	(Nm)	(Nm)		
25	Valve		-1075	-100	-1272		8737		
100	Valve	-47 230	3590 1663	-100 28	-1272 25	-482 -123	7954 883		
105	valve	230		28	25	-112	-100		
		(T. 7.F.						pe force	global coordinates: Sustained (W+P)
Node	FX	FY	FZ	MX	MY	MZ			
	(N)	(N)	(N)	(Nm)	(Nm)	(Nm)			
5	-100		47	-319	-392	214	1		
10	100	-3511		319	383	504			
10	-100	2827		-319	-383	-504			
15A 15A	100 -100	3132 -3132		319 -319	23	-670 670	1		
15A 15B	100	3595		337	-23 5	-1889			
15B	-100	-3595		-337	-5	1889	1		
20A	100	8074		608	5	-1310			
20A	-100	-8074	_	-608	-5	1310			
20B	100	8537	-47	3814	-33	-1272			
20B	-100	4746		-3814	33	1272			
25	100	-1759 -4274	_	-8737 7054	_	-1272 1272			
30 35	-100 100	4506	-47	7954 -6637	482 -512	-1272			
35	-330	-3613	-	6612	350	-1239			
40	330	3845		-5494		1239			
40	-330	-3845		5494	449	-1239			
45	330	4196		-3363	_	1239			
45	-330	-4196	2.0	3363	624	-1239			
50	330	5368	-19	6679	-1316				
35	230	-894	28	25	162	2511			
100	-230	1432	-28	-25	-123	-883			

Caepi	pe								Sar	ple Problem 2	Page
- 31			e e	-/-			Р	ipe force	s in globa	coordinates: Sustained (W+P)	
Node		FY	FZ	MX (Nex)	MY (Nim)	MZ	0				
105	(N) 230	(N) -3446	(N) 28	(Nm) 25	(Nm)	(Nm	-				
110A	-230	3456	-28	-25	-111	191	3				
110A	230	-3456		25	111	-191	7				
110B	-230	3594	-28	-19	-105	940					
110B	10000000	-3594	D3200	19	105	-940	8				
115A		4551	-28	50	-105	368					
115A 115B	230 -230	-4551 4689	28 -28	-50 56	105 -98	-368 1376	9.04				
115B		1260	28	-56	98	-137	_				
120A	-230	231	-28	56	9	-623					
120A	230	-231	28	-56	-9	623					
	-230	347	-28	52	15	-521					
120B		-347	28	-52	-15	521					
125	-230	1727	-28	-45	39	1179					
10	-	mar	-	Lee	Lance		-	ther force	s in globa	I coordinates: Sustained (W+P)	
Node	Туре	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)	4			
25		-100	1075	_	8737	419	1272	_			
30	vaivo	100	3590	-47	-7954	-482	-127				
100	Valve	230	-1663	_	25	123	883				
105		-230	3215	-28	-25	-112	100	les.			
								0	isplacem	ents: Sustained (W+P)	
				isplace	-		_	.1			
	X (mm	-		Z (mm)				g) ZZ (d			
5	0.000	0.0		0.000	0.00		0.0143	_			
10	0.000	-0.1	-	-0.051	0.00	-	0.0147	-	-		
15A 15B	0.003	2.1	_	-2.618	0.01	-	0.0215	-			
20A	-0.401	_	-	-2.650 -0.248	0.01	-	0.0199	-	_		
20B	-2.816	_		0.000	0.06		0.0270	_	-		
25	-1.087	_		0.000	0.00	_	0.0232	_	-		
30	-0.837	_	-	0.000	0.00	_	0.0229	_			
35	-0.719	_	_	0.000	-0.0	-	0.0222	_	-		
40	-0.604	_	-	0.000	-0.0	-	0.0217	-	-		
45	-0.411	_	-	0.000	-0.0	-	0.0199	-	and the last of		
50	0.000	0.0		0.000	0.00	_	0.0000	-	A CONTRACTOR OF THE PARTY OF TH		
100	-0.720	-		0.478	-0.0	-	0.0172	-			
105	-0.720	1.1	02	0.598	-0.0		0.0169	_	35		
110A	-0.720	1.1	50	0.606	-0.0	079	0.0168	-0.10	35		
110B	-0.389	1.5	28	0.628	-0.0	102	0.0128	-0.06	46		
	1.397	1.5	43	0.190	-0.0	-	0.0043	and the latest designation of the latest des			
	1,454	1.5	ed minimizer of	0.166	-0.0	CONTRACTOR OF THE	0.0016	and the latest designation of			
_	1.453	-0.3	_	0.064	-0.0	_	-0.0028	_			
_	1.418	-0.3	_	0.056	-0.0	_	-0.0032	_			
125	0.000	0.0	00	0.000	0.00	00	0.0000		_		
			Lec			Lance				nchors; Expansion (T1)	
_	Tag F		FY (Z (N)	_			MZ (Nm)		
50	-	1103	-161	-	072	297			334		
125	<u> </u>	2003	76		49	-749	18	39	5329	Second Europeian (T4)	
Ned	T1-	Name -	-		In-	7.4	LAND.	LC	ads on H	angers: Expansion (T1)	
Node 20B	Tag 1		_	Load (N	_	-	(N)				
	1 15	Jser ha	iger		1	83	_				
115B	1	Srinnell	- 4	696	1	696					

Саері	pe								Sample Problem 2	Page 1
	- 10		a	0.40	2.0			- 1	oads on Nozzles: Expansion (T1)	
lode	Tag A		y Shea	r z Sh	ear T	orque	Circ.M	lom L	ong Mom	
	-	N)	(N)	(N)	_	lm)	(Nm)	_	Nm)	
	-	1099	-724	694	-1	823	-639	_	2330	
110					l l	1	<u> </u>		rces in local coordinates: Expansion (T1)	
Node	(N)	fy (N)	fz (N)	mx (Nm)	my (Nm)	mz (Nm)	SIF	SE (MPa)		
;	-1099	-	-724	-1823	-	-639		6.320		
10	-1099	C022430	-724	-1823		-500	1.00	6.041		
10	-1099	-694	-724	-1823		-500	1.00	6.041		
15A	-1099	-	-724	-1823	_	-	0.54	12.76		
15A 15B	-1099 -694	-694 1099	-724 -724	-1823 -3661	-3385 1547		2.54 2.54	32.18 31.93		
15B	-694	1099	-724	-3661	1547	4686	2.03	12.63	1	
20A	-694	1099	-724	-3661	-2641			9.916		
20A	-694	-724	-1099	-3661	-1676		2.54	25.04		
20B	-724	694	-1099	-	_	-	_	_		
20B 25	-724 -724	-611 -611	1099	-2095 -2095		-2652 -295	100000	9.651 4.870		
30	-724	-611	1099	-2095	_	85	1.00		1	
35	-724	-611	1099	-2095	1.0000000	268	MACH COCK	14.89		
35	-1072		3103	-334	320	769	2.49	4.692		
04	-1072	and the latest and th	3103	-334	1251	721	0.00	3.164		
40 45	-1072 -1072		3103 3103	-334 -334	1251 2896	721 635	2.00	6.189 21.86		
15	-1072	and the last of	3103	-334	2896	635	2.00	11.03		
60	-1072		3103	-334	9411	297	9.5 - 10	34.40		
35	-2003		-349	-501	1693	1761				
100	-2003		-349	-501	1205	2841	-	23.02		
105 110A	-2003 -2003		-349 -349	-501 -501	1064 1055	3153 3173	1.00	24.73 24.84		
110A	-2003	100000	-349	-501	1055	3173	2.17	53.15		
110B	CONTRACTOR	2003	-349	975	421	2892		48.13		
110B	0.70100000	-2003		975	-421	-2892		22.34		
115A		-2003	-	975	448	2102	2.17	17.17 36.93		
115A 115B		-00000	349 349	975 528	448 -895	100000000000000000000000000000000000000	2.17	41.01		
115B	-	-76	-349	528	895	-2384	-	19.24	1	
120A	mirror market	-	-349	528	-459	-2087	-	16.37		
120A	Marie No.		349	528	459		2.17	34.79		
120B 120B		1963 -1963	349	633	-324 324	-1723	_	29.10	1	
125	-409	-1963		633	-929	5329		39.23		
10	- 01		10 1				(orces in local coordinates: Expansion (T1)	
		fx		fz	mx	my	mz	T		
_	Туре	(N)	(N)	(N)	(Nm)	(Nm)	(Nm)			
25 30	Valve	-724 -724	-611 -611	1099 1099		1000 1684	-295 85	3		
100	Valve	-2003	_	-349	-501	1205	2841			
105	3.000	-2003		-349	-501	1064	3153			
		110					F	ipe for	ces in global coordinates: Expansion (T1)	
Node	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)				
5	1099	694	724	1823	-2330	-	1			
10	-1099	12 March 1 4	-724	-1823						
0	1099	694	724	1823	-2186	500	1			
5A	-1099	_	-724	_	_	4840				
15A	1099	694	724	1823	10000	4840				
15B	-1099 n 7.60	-034	-724	-134/	-3001	4686			Sample2	Sep 12,20

	ipe						1997	- for	Sample Problem 2 Pa
		-	_	lee-	lee-	L	Pip	e forces in	in global coordinates: Expansion (T1)
Node	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)			
15B	1099	694	724	1547	3661	-4686	1		
20A	-1099	-694	-724	2641		-1676			
20A	1099	694	724	-2641	3661	1676	1		
20B	100000000000000000000000000000000000000	-694	-724	2652	-3242	N *** () ** () ()			
20B	1099	611	724	-2652	3242	2095	1		
25	-1099	-611	-724	295	1000	-2095			
30	1099	611	724	85		2095			
35		-611	-724	-268	2014	-2095			
35 40	3103 -3103	-161	1072 -1072	769 -721	-320 1251	334 -334			
40	3103	161 -161	1072	721	-1251	-	1		
45		161	-1072		2896	-334			
45	3103	-161	1072	635	-2896		1		
50		161	-1072	-297		-334			
35	-2003	772	-349	-501		1761	1		
100	2003	-772	349	501	1205	-2841			
105		772	-349	-501	100 CV 12	3153			
	_	-772	349	501	_	-3173	4		
110A	-2003 2003	772	-349	-501	-1055 975	3173			
7 - 1 - 1		-772 772	349	421	_	-2892	1		
	-2003 2003	-772	-349 349	-421 -448	-975 975	2892			
	-2003		-349	448	-975	-2102	1		
		-772	349	-528	895	2384			
115B	-	76	-349	528	-895	-2384	1		
120A	2003	-76	349	-528	-459	2087			
		76	-349	528	459	-2087			
		-76	349	-468	-536	1723	1		
	-2003		-349	468	536	-1723			
125	2003	-76	349	749	-839	-5329	_		
		Address of the last of the las						er forces i	in global coordinates: Expansion (T1)
Mada	Tomas	FX	FY	FZ	MX	MY	MZ		
Mode	_	(N)	(N)	(N) 724	(Nm) -295	(Nm) -1000	(Nm) 2095		
	Maken								
25	Valve	200-01-121	611	CC50000000	400000000000000000000000000000000000000	5000 5.50	5200 - 000		
25 30	G200000	-1099	-611	-724	-85	1684	-2095		
25	Valve	200-01-121	-611 772	CC50000000	400000000000000000000000000000000000000	5000 5.50	-2095		
25 30 100	G200000	-1099 -2003	-611 772	-724 -349	-85 -501	1684 -1205	-2095 2841	Disp	splacements: Expansion (T1)
25 30 100	G200000	-1099 -2003	-611 772 -772	-724 -349 349	-85 -501 501	1684 -1205 1064	-2095 2841	Disp	splacements: Expansion (T1)
25 30 100 105	Valve	-1099 -2003 2003	-611 772 -772	-724 -349 349 splacer	-85 -501 501 ments (1684 -1205 1064 global)	-2095 2841 -3153		
25 30 100 105 Node	Valve X (mm	-1099 -2003 2003	-611 772 -772 Di	-724 -349 349 splacer Z (mm)	-85 -501 501 ments (1684 -1205 1064 global) (deg)	-2095 2841 -3153 Y (deg)	ZZ (deg)	
25 30 100 105	Valve	-1099 -2003 2003) Y (-611 772 -772 Dimm)	-724 -349 349 splacer	-85 -501 501 ments (1684 -1205 1064 global) (deg) 1	-2095 2841 -3153		0
25 30 100 105 Node 5	X (mm	-1099 -2003 2003) Y (i 0.0	-611 772 -772 -772 Dimm) 00	-724 -349 349 splacer Z (mm) 0.000 -0.301	-85 -501 501 ments (XX (0.00	1684 -1205 1064 global) (deg) \() 000 (0	-2095 2841 -3153 Y (deg)	ZZ (deg) -0.1468	
25 30 100 105 Node 5	X (mm -0.027 0.530	-1099 -2003 2003) Y (0 -0.0 5 -17	-611 772 -772 -772 Dimm) 00 514 .418	-724 -349 349 splacer Z (mm) 0.000 -0.301 -12.775	-85 -501 501 ments (0.00 -0.0	1684 -1205 1064 global) (deg) \(\)	-2095 2841 -3153 Y (deg) 0.0851 0.0871	ZZ (deg) -0.1468 -0.1473	
25 30 100 105 Node 5 10 15A 15B	X (mm -0.027 0.530 21.975	-1099 -2003 2003) Y (0 0.0 -0.5 5 -17 9 -16	-611 772 -772 -772 Dimm) 00 514 .418	-724 -349 349 splacer Z (mm) 0.000 -0.301	-85 -501 501 ments (0.00 -0.0 i -0.0 i -0.0	1684 -1205 1064 global) (deg) \(\) 000 (0 021 (0 823 (0 828 (0	-2095 2841 -3153 YY (deg) .0851	ZZ (deg) -0.1468 -0.1473 -0.0739	
25 30 100 105 Node 5 10 15A 15B 20A	X (mm -0.027 0.530 21.975 23.089	-1099 -2003 2003 Y (0 -0.5 -17 9 -16 2 -0.4	-611 772 -772 -772 Dimm) 00 514 .418 .606	-724 -349 349 splacer Z (mm) 0.000 -0.301 -12.775 -13.625	-85 -501 501 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00	1684 -1205 1064 global) (deg) V 000 0 021 0 823 0 828 0 689 -	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277	
25 30 100 105 Node 5 10 15A	X (mm -0.027 0.530 21.975 23.085 16.972	-1099 -2003 2003 Y (0 -0.5 -17 9 -16 2 -0.4	-611 772 -772 Dimm) 00 514 .418 .606 183	-724 -349 349 splacer Z (mm) 0.000 -0.301 -12.775 -13.625 -22.202	-85 -501 501 ments (0.00 -0.0 i -0.0 i -0.0	1684 -1205 1064 global) (deg) 1 000 (021 (823 (828 (689 -	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668 0.0337	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660	
25 30 100 105 Node 5 10 15A 15B 20A 20B	X (mm -0.027 0.530 21.979 23.089 16.977	-1099 -2003 2003 Y (0 -0.5 -17 9 -16 2 -0.4 1 0.7	-611 772 -772 -772 00 514 .418 .606 883 90 25	-724 -349 349 splacer Z (mm) 0.000 -0.301 -12.775 -13.625 -22.202 -21.467	-85 -501 501 ments (0.00 -0.0 -0.0 -0.0 -0.0	1684 -1205 1064 global) (deg) 1 000 (0 021 (0 823 (0 828 (0 689 -	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668 0.0337 0.0874 0.1184	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660 0.0627	
25 30 100 105 Node 5 10 15A 15B 20A 20B 25 30	X (mm -0.027 0.530 21.979 23.089 16.972 15.891 6.856	-1099 -2003 2003 Y (0 -0.5 -17 9 -16 2 -0.4 1 0.7 0.5	-611 772 -772 -772 Dimm) 00 514 .418 .606 183 90 25	-724 -349 349 splacer Z (mm) 0.000 -0.301 -12.775 -13.625 -22.202 -21.467 -10.718	-85 -501 501 ments (0.00 -0.0 -0.0 -0.0 -0.0 -0.0	1684 -1205 1064 global) (deg) V 000 0 021 0 823 0 828 0 689 - 120 - 30 -	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668 0.0337 0.0874 0.1184 0.1374	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660 0.0627 0.0165	
25 30 100 105 Node 5 10 15A 15B 20A 20B 25 30 35	X (mm -0.027 0.530 21.979 23.089 16.973 15.891 6.856 5.368	-1099 -2003 2003) Y (0 -0.5 -17 9 -16 2 -0.4 1 0.7 0.5 0.3	-611 772 -772 -772 00 514 .418 .606 183 90 25 83 15	-724 -349 349 splacer Z (mm) 0.000 -0.301 -12.775 -13.625 -22.202 -21.467 -10.718 -8.993	-85 -501 501 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00 -0.00	1684 -1205 1064 global) (deg) \(\) (00 0 021 0 823 0 828 0 689 - 120 - 131 - 28 -	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668 0.0337 0.0874 0.1184 0.1374 0.1364	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660 0.0627 0.0165 0.0145	
25 30 100 105 Node 5 10 15A 15B 20A 20B 25 30 35	X (mm -0.027 0.530 21.975 23.085 16.972 15.895 6.856 5.368 4.658	-1099 -2003 2003 2003) Y (0 -0.4 -0.5 -17 9 -16 2 -0.4 1 0.7 0.5 0.3 0.3	-611 772 -772 00 00 00 514 4.418 .606 183 90 25 883 115	-724 -349 349 349 -72 (mm) 0.000 -0.301 -12.775 -13.625 -22.202 -21.467 -10.718 -8.993 -8.157	-85 -501 501 501 XX (0.00 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.	1684 -1205 1064 1206 1064 106	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668 0.0337 0.0874 0.1184 0.1374 0.1364 0.1340	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660 0.0627 0.0165 0.0145 0.0109	
25 30 100 105 Node 5 10 15A 15B 20A 20B	X (mm -0.027 0.530 21.975 23.089 16.972 15.896 5.368 4.658 3.956	-1099 -2003 2003 0.0 -0.5 -177 0.5 -107 0.5 0.3 0.3 0.3	-611 772 -772 -772 -772 -772 -772 -772 -77	-724 -349 349 349 0.000 -0.301 -12.775 -13.625 -22.202 -21.467 -10.718 -8.993 -8.157 -7.322	-85 -501 501	1684 -1205 1064 -1205 1064 10	-2095 2841 -3153 Y (deg) 0.0851 0.0871 0.0668 0.0337 0.0874 0.1184 0.1374 0.1364 0.1340 0.1330	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660 0.0627 0.0165 0.0145 0.0109	
25 30 100 105 Node 5 10 15A 15B 20A 20B 25 30 35 40	X (mm -0.027 0.530 21.975 23.086 16.972 15.894 6.856 4.658 3.956 2.747	-1099 -2003 2003 2003 V (0.0 -0.5 5 -17 0.5 0.3 0.3 0.2 0.1	-611 772 -772 000 0514 .418 .606 .683 990 925 552 000	-724 -349 349 349 -0.000 -0.301 -12.775 -13.625 -22.202 -21.467 -10.718 -8.993 -8.157 -7.322 -5.846	-85 -501 -501 -501 -501 -501 -501 -501 -50	1684 - 1205 1064 10	-2095 2841 -3153 YY (deg) 0.0851 0.0871 0.0668 0.0337 0.0874 0.1184 0.1374 0.1364 0.1340 0.1330 0.1259	ZZ (deg) -0.1468 -0.1473 -0.0739 0.0277 0.0660 0.0627 0.0165 0.0145 0.0109 0.0104	

Caepi	pe									ple Problem 2 Page
-									Displace	ents: Expansion (T1)
	W /	1 Tv		Displace					724	
_	X (mr		mm)	Z (mm)	_	(deg) 1378		_	Z (deg)	
110A	-0.46 -0.63	_	20000				2000		0.0798	
_	12.29			_	1.2826					
_	12.28	_	275	-7.778	_		0.066	_	.1495	
and the same of	-4.04	_	860	-1.789	-	nimen in committee	0.087	-	0683	
120B	-4.57	_	715	-1.455	-0.	0085	0.078	6 0.	1626	
125	0.000	0.0	00	0.000	0.0	0000	0.000	0 0.	0000	
CVLST-115			A1		No.			Lo	oads on An	rs: Operating (W+P1+T1)
Node	Tag	FX (N)	FY	(N) F	Z (N)	MX	Nm)	MY (N	m) MZ (Nn	
50	\rightarrow	2773	-552	_	091	-638	-	-8095	-905	
125	Ш	-1774	-165	51 3	321	-704		800	4149	
								Lo	ads on Ha	rs: Operating (W+P1+T1)
and the latest designation of	Tag			Load (N	-	-	meterators			
20B	\rightarrow	User ha	_		1	-132	-			
115B	Ш	Grinnell	- 1	5254	1	-525	4	- 2	anda es Mi	Consider Michaelle
Mark	Te :	Audat	Luca			Faster	I c			es: Operating (W+P1+T1)
Node	Tag	Axial (N)	y Sho (N)	ar z Si (N)		Nm)	(Nm	Mom	Long.Mon (Nm)	
5	_	-999	-770	436	_	1504	-853	_	-2722	
	_						Pi	pe forc	es in local	ordinates: Operating (W+P1+T1)
Node	fx	fy	fz	mx	my	mz	SIF	_		
	(N)	(N)	(N)	(Nm)	(Nm)	(Nm		(MP		
5	-999	-4360		-1504			1	13.8		
10	-999	-4205	-	-1504	_	_	_	0 13.3	_	
10 15A	-999 -999	-3520 2438	-770 -770	-1504 -1504		2 4170	1.0	18.5	2001	
15A	-999	2438	-770	-1504	_	2 4170	-	-		
15B	2901	999	-770	-3656	1210			4 25.2	21	
15B	2901	999	-770	-3656	1000			17.4	955	
20A	7380	999	-770	-3656	-	8 -298	_	20.0	-	
20A 20B	7380 -770	-770 -7844	-999 -999	-3656 -3367	3275	6 3248				
20B	-770	-5356	-	-3367		-	_	23.5	and the same	
25	-770	-2370	0.000	-3367		8442		0 25.8		
30	-770	3664	999	-3367	100000		200.0		1000	
35	-770	3896	999	-3367	_	_	_	9 43.7		
35 40	9.90000		2773 2773		-30 802	7381 6214		20.1		
40	-1091	_	2773	_	802	6214	_	_		
45	NO. 10 Sec. 1	4357	2773		2272				200	
45		4357	2773		2272			23.5		
50	-	5529	2773	-	8095	_	_	44.0	-	
35 100	-1774		-321 -321	-476 -476	1532	DOLLARS SEE		01 5700 0 1		
105	-1774	_	-321	-476	952	3052	_	0 41.6		
0.0000000000000000000000000000000000000	-1774		-321	-476	944	2982		41.1	000	
	-1774		-321	-476	944	2982				
-	2822	-	-321	870	402	1951	_	-	mining	
	2822 3779	-1774 -1774		870 870	-402 398	-195 2470		35.3		
	3779			870	398	2470	_	_		
	-1774			472	-797	3759		2000	5.55	
	-1774	-1337	-321	472	797	-375	_	46.2		
120A	-1774	154	-321	472	-450	-146	4	29.9	95	

Caepi	Je.						PR-C	t.	Sample Problem 2	Page 1
									n local coordinates: Operating (W+P1+T1)	
Node	fx (N)	fy (N)	fz (N)	mx (Nm)	my (Nm)	mz (Nm)	SIF	Sopr (MPa)		
20A	-1774	-154	321	472	450	1464	2.17	42.50		
120B	-691	_	321	606	-278	1202	2.17	38.41		
120B	-691	-1656		606	278	-1202		28.61		
125	-2030	-1323	-321	606	-876	4149		49.14 r force:	in local coordinates: Operating (W+P1+T1)	
		fx	fy	fz	mx	my	mz	T	minous consumates operating (11 - 1 - 1 - 1)	
Node	Embourge Street	-	(N)	(N)	MATERIAL PROPERTY.	(Nm)	(Nm)			
255 CV	Valve		-1685 2979	K1197253		581 1202	8442 8039			
30 100	Valve	Minimum	891	999 -321	-3367 -476	-	3725			
105	AGIAC		2443	-321	-476	952	3052			
				× ×			Pipe	forces	global coordinates: Operating (W+P1+T1)	
Node	100.000	FY	FZ	MX	MY	MZ				
	(N)	(N)	(N)	(Nm)	-	(Nm)				
10	999 -999	4360 -4205	770 -770	1504 -1504	-2722 2568	853 4				
10	999	3520	770	1504	-2568	-4	1			
15A	-999	-	-770	-1504	-3362	Technology (Control				
15A 15B	999 -999	-2438 2901	770 -770	1504 -1210	3362 -3656	-4170 2797				
_	999	roministration in the	770	1210	3656	-2797				
20A	-999		-770	3248		-2986				
500131	999	-7380		-3248		2986	1			
20B	-999	7844		6466		-3367				
20B 25	999 -999	5356 -2370	770 -770	-6466 -8442	3275 581	3367 -3367				
30	999	-3664	_	8039	-1202	3367				
35	-999		-770	-6905	1502	-3367				
2000 ST	2773	-3774		7381	30	-905				
40 40	-2773 2773	4006 -4006	-1091	-6214 6214	802 -802	905				
45	-2773		-1091	-3998	2272	905				
45	2773	-4357	1091	3998	-2272	-905				
50	-2773	THE REAL PROPERTY.	-1091	6382	8095	905				
2012/01/11	-1774 1774	-122 660	-321 321	-476 476		4272 -3725				
_	-1774	-2674	_	-476	-952	3052				
110A	1774	2684	321	476	944	-2982				
		-2684		-476		2982				
_		2822 -2822	321	402 -402	870 -870	-1951 1951	-			
	-1774 1774	3779		-398	870	2470				
	-1774	-3779		398	-870	-2470				
115B	1774	3917	321	-472	797	3759				
	-1774 1774	1337	-321 321	472	-797 -450	-3759 1464				
_		154 -154	-321	-472 472	-450 450	-1464				
V965 1 5%	1774	271	321	-416	-521	1202				
	-1774	-271	-321	416	521	-1202				
125	1774	1651	321	704	-800	-4149	Other	fores	n global constitutos: Operation AVA D1 + T1)	
		EV	EV	E7	MY	MV		orces	n global coordinates: Operating (W+P1+T1)	
Node	Туре	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)			
25	Valve		1685	770	8442	-581	3367			
30		-999	2979	-770	-8039		-3367			

Caepi	pe									Sample Problem 2	Page 1
-				115			Oth	er for	es in glo	bal coordinates: Operating (W+P1+T1)	
		FX	FY	FZ	MX	MY	MZ				
	Туре	(N)	(N)	(N)	(Nm)	(Nm	_				
100	Valve	The contract of		-321	-476	-108					
105		1774	2443	321	476	952	-30	_	Disabase		
	_								Displace	ments: Operating (W+P1+T1)	
Marke.	V /	. Iv		Displacer					7 (4.00)		
named to the last	X (mn	-	(mm)	Z (mm)	market in the last of	NAMED BY	-	-	Z (deg)		
5	-0.024	_	000	0.000	0.00	-	0.099	_	1960		
10	0.533	_	688	-0.352	_		0.101	_	0.1963		
15A	21.97		5.229	-15.393	_	679	0.088	-	.0036		
15B	22.68	-	3.955	-16.274	_	645	0.053	-	0749		
20A	13.98	_	191	-22.450	-	386	-0.06	_	0725		
20B	13.07	_	158	-21.467	-	-	_	-	0536		
25	5.769	_	926	-10.718	-	-	-0.11	_	0.0206		
30 35	4,531 3,939	_	134	-8.993 -8.157	0.0	-	-0.11	-	0.0238		
40	3.352	_	191	-7.322	_	028	-0.11	_	0.0296		
45	2.337	_	070	-5.846	_	202	-0.10	_	0.0241		
50	0.000	-	000	0.000	0.00	-	0.000		0000		
100	0.046	_	323	-10.293	-		-0.06	-	1723		
105	-1.07	_	570	-10.747	_	-	-0.06	_	0.1812		
110A	-1.182	_	554	-10.776	_	_	-0.06	_	0.1832		
110B	-1.025	_	67	-10.767	_		-0.02	_	0.3224		
115A	_	_	.069	-8.055	0.08	_	0.045	_	0.3062		
115B		-	837	-7.611	0.05	-	0.068	-	1.1322		
120A	-2.596	_	.483	-1.724	-	-0.0044		_	0753		
120B	-3.157	_	16.357 -1.398		-	-0.0090		-	1419		
125	0.000	0.0	000	0.000	0.00	000	0.000	0 0	0000		
									Load	s on Anchors; Seismic (g)	
Node	Tag	FX (N)	FY	(N) F2	Z (N)	MX	(Nm)	MY (N	m) MZ	Nm)	
50	_	3874	282		192	841	_	10805	_		
125		1274	622	79	98	211	-	734	270	3	
- 50	- 1		97.5	175	- 1				Load	ls on Hangers: Seismic (g)	
Node	Tag	Type	-	Load (N)	No of	Tota	I (ND			and the state of t	
20B	_	User ha	_	1548	1	154	_				
115B	\rightarrow	Grinnel	_	192	1	192					
					-	1	_		Loar	ds on Nozzles: Seismic (g)	
Node	Tag	Axial	Ty She	ear z Sh	earT	orguse	Circ	Mom	Long.N		
		(N)	(N)	(N)		im)	(Nm		(Nm)		
5		3856	1764		2 2	908	539		3676	7	
							-	Pi	e forces	in local coordinates: Seismic (g)	
Node	fx	fy	fz	mx	my	m	z I	-	SL+SO		
	(N)	(N)	(N)	(Nm)			lm)		(MPa)		
5	3856	end Administration			367	-	39		18.63		
10	3809	1105	-	manufacture in contract of	-	-	_	1.00	AND DESCRIPTION OF THE PARTY OF		
10	3604	985	151			2.50		1.00			
15A	1820	610	340	_	_		268		20.41		
15A	1820	610	340	b. P475070703					32.00		
15B	667	1681	-		_	-	_	2.54			
15B 20A	667 1425	1681 364	463 177		1000	6000	765 427		22.16		
20A	1425	1777	_	_	_	_		2.54			
	0.0000000000000000000000000000000000000										
_	-	-		_	_	_	_	$\overline{}$			
25	2809	1 5/1000	721					1.00			
20B 20B	1916 1916	1513 477	245 245	2517 2517	200	2 4	576 576	2.54	44.97 27.23		

Caepi	pe									Sample Problem 2	Page
			1					-		in local coordinates: Seismic (g)	
Node	fx (N)	fy (N)	fz (N)	mx (Nm		ny (Nm)	mz (Nm)	SIF	SL+SO (MPa)		
30	4616	1837	_	-	_	1989	2564	1.00	32.81		
35	4686	1882				2365	2631		50.26		
35	5966	2478	25000	100		332	1516	2.49	42.14		
40	6036	2523	_	_	_	1331	1898	0.00	25.27		
40 45	6036	2523 2591		e control	6. III.	1331	1898 2971		33.84 52.28		
45	6141	2591	-	-	-	3083	2971	2.00	37.47		
50	6492	2820	75500	1.0000	20 10	10805			83.02		
35	761	631	1297	- 1000		2223	1152	5.00	58.02		
100	599	532	1139	-	_	961	700	-	24.27		
105 110A	10	242	564 561	111		874 871	652 647	1.00	31.30 31.78		
110A	_	242	561	111	-	871	647	2.17	-		
110B	0.000	50	524	852		998	601		47.86		
110B	235	50	524	852	9	998	601		37.15		
115A		337	301	852	2	275	302		29.82		
115A		337	301	852	9.0	275	302		35.78		
115B 115B		287	278	302	-	315	279 279	2,17	45.85 35.57		
120A		362	395	302		815 237	1026		31.58		
120A	_	362	395	302	-	237	1026	2.17	39.29		
120B		782	423	301		276	951		37.18		
120B		782	423	301	100	276	951		30.19		
125	773	1189	798	301	2	2221	2703	_	52.40		
					_	1		0	ther force	s in local coordinates: Seismic (g)	
Node	Туре	fx (N)	fy (N)		nx Nm)	my (Nm)	mz (Nm)				
25	Valve				517	-		8			
30		4411			517		2564				
100	Valve	530	1770		117		700				
105	- 8	65	261	627 1	117	874	652				
					_			P	pe forces	in global coordinates: Seismic (g)	
Node	FX (N)	FY (N)	FZ (N)	MX (Nm		MY Nm)	MZ (Nm)				
5	3856	1132	and interestant	-	-	3676	539	ł			
10	3809	1105	100000			3340	358	l			
10	3604	985	1514	_	_	3340	358	1			
15A	1820	610	340	290	8 1	1979	4268	1			
15A	1820	610	340	290		1979	4268				
15B	1681	667	463	278	_		3765	1			
15B 20A	1681 364	667 1425	463 1777	7 410	0.0	1917 1917	3765 2427	ſ			
20A	364	1425	-	-	-	1917	2427	1			
20B	245	1513	250.00	6 (4 5 700 7	900	2002	2517	Į.			
20B	245	477	1916	457	6 2	2002	2517	1			
25	721	741	2809	-	-	1868	2517				
30	2519	1837	100000	GC WAR	52	1989	2517	l			
35 26	2589	1882	-	-	-	2365	2517	1			
35 40	3348 3418	2523	3.07	54 033		632 1331	1467				
40	3418	2523	-	ACCRECATE VALUE OF THE PARTY NAMED IN	-	1331	1467	1			
45	3523	2591		20.0		3083	1467	1			
45	3523	2591	_	_	\rightarrow	3083	1467	1			
50	3874	2820	_	_	-		1467	1			
20.	761	631	129	111	7 2	2223	1152	ı			
35 100	599	532	1139	111		961	700				

Caepi	pe								Sai	nple Problem 2	Page
		154	741	110			4.	Pipe f	orces in gl	obal coordinates: Seismic (g)	
Node		FY	FZ			MY	MZ		-		
	(N)	(N)	(N)	_	_	(Nm)	(Nm)				
105	10	242	564			874	652	l			
110A 110A		242	56	_	_	871 871	647	8			
110B		235	524			852	601	l			
110B	_	235	524	_	-	852	601				
115A		271	301	22 1033	0.000	852	302	L			
115A	337	271	301	1 27	75	852	302	ľ			
115B	378	287	278	30	12	815	279				
115B	DAYSSEE	233	278			815	279				
120A	-	362	395	_		237	1026	l.			
120A	135575	362	395	200	V2010-1	237	1026	ľ			
120B	_	696	423	_	-	359	951	ł			
120B 125	1340	318 463	423 798			225 244	951 2703				
		1	11.00					Other	forces in g	obal coordinates; Seismic (g)	
		FX	FY	FZ	MX	MY	MZ				
	Type	(N)	(N)	(N)	(Nm) (Nm)				
25	Valve		850	3014							
30		2314	1705		_		9 2517				
100	Valve	530 65	491 261	627		7 961 7 874					
100	_	00	201	1027	1111	Jose	002		Displac	ements: Seismic (g)	
- 2				Displac	ceme	nts (al	nhal)		Dispiac	cinenta, Setariac (g)	
Node	X (mn	i Iv	(mm)	Z (m				deg) ZZ (dea)		
5	0.094	-	000	0.00	_	0.000					
10	0.095	-	434	0.47	_	0.003	_	_			
15A	0.109	_	.039	20.5	$\overline{}$	0.131	-	-	-		
15B	0.975	-	601	20.3	$\overline{}$	0.172	-	-			
20A	17.24	3 15	.597	1.12	1	0.185	8 0.11	25 0.14	60		
20B	17.28	8 14	.745	0.02	4	0.137	2 0.13	54 0.10	94		
25	7.646	6.	236	0.01	8	0.125	9 0.15	04 0.05	46		
30	6.012	4.	873	0.01	7	0.125	4 0.15	0.05	22		
35	5.226	4.	220	0.01	6	0.123	8 0.14	88 0.04	80		
40	4.445	3.	574	0.01	5	0.122	1 0.14	79 0.04	155		
45	3.099	2.	471	0.01	3	0.114	5 0.14	06 0.03	90		
50	0.000	0.	000	0.00	0	0.000	0.00	00.00	000		
	5.227	_	313	3.19	-	0.105	_	_			
	5.227	4.	370	4.00	-	0.104	-		33357		
	5.227	_	374	4.05	_	0.104					
	5.213		380	4.50	$\overline{}$	0.102					
-	4.219	\rightarrow	379	6.82	$\overline{}$	0.107	-	and the local division in the local division	_		
-	4.135	\rightarrow	224	7.11	\rightarrow	0.100	-	Marian Property			
	4.132	_	197	4.38	-	0.089					
	3.937	_	977	3.95	_	0.086	_		200		
125	0,000	10/	000	0.00	v	0.000	0.00	00.00		on Brokers Mind	
	T. 1	DV AV	Ten:	0.0	en.	. I.	100 (01)	lane na		on Anchors: Wind	
	Tag I		_	(N)	FZ (_			MZ (Nm)		
50	\rightarrow	205	-15		148	\rightarrow	649	-3795	-662		
125	اللا	92	13	8	-91		228	163	-993		
0-1	T. I.			1 - 1	an In		Total this		Loads	on Hangers: Wind	
	Tag			_	_	_	Total (N)	4			
20B	L 19	Jser ha	-	-159 1	1	-	159				
115B		Srinnel									

Caepi	pe								Sar	Problem 2 Page 1
-		ė.		1.0					Loads	lozzles: Wind
Node	Tag			ar z Sh			Circ.M		Long.Mom	
5	-	(N) 844	(N) -57	(N) -207	_	_	(Nm) -1	$\overline{}$	(Nm) 184	
			1 21	124	_			_		al coordinates: Wind
lode	fx	fy	fz	mx	my	mz	SIF	SL+S	so	
	(N)	(N)	(N)	(Nm)	(Nm)	(Nm)		(MPa	-	
in	844	207	-57	-314	-184	-1	1 00	9.349	7005	
10	844	207	-57 -57	-314	-195 -195	-43 -43	1.00	9.692	-	
5A	844	207	-57	-314	-631	-1636		12.64	50.5	
15A	844	207	-57	-314	-631	-1636		17.30	900	
15B	207	-844	-57	-653	292	-1393	_	21.40	-	
15B 20A	207	-430 -430	-57 -57	-653 -653	292 -35	-1393 1094		14.97 13.99		
20A	207	-57	-23	-653	1094	-	2.54	19.01		
20B	-57	-207	-23	1085	644	136		27.92		
20B	-57	48	337	1085	-644	-136	36 3	18.16	0.85	
25	-57	48	337	1085	658	-322	1.00	28.07	_	
30 35	-57 -57	48 48	745 745	1085 1085	1074		1.00	27.03 39.73	2000	
35	-148	152	853	662	798	-204	-	-	_	
01	-148	152	853	662	1054	-	-8081	21.50	-	
40	-148	152	910	662	1054	0.000	2.00			
15	-148 -148	152	910	662 662	1536 1536	-	2.00	35.82 26.12	and the same of th	
50	-148	152	1075	662	3795			46.02	200	
35	-65	-104	-91	-163	500	-423	2.49	37.45	5	
100	-65	-104	-91	-163	372	-278	-	15.94		
105 110A	-65 -65	-104 -104	-91 -91	-163 -163	335 332	-236 -233	1.00	23.27		
110A	-65	-104	-91	-163	332	-233	2.17	26.71		
110B	100000	65	-91	312	142	-224		35.77		
110B	J-200220014	67	91	312	-142	224	00000	29.69	200	
115A	_	67	91	312	86	57	0.47	25.35	-	
115A 115B	Del 2777	216 104	91 91	312 107	86 -291	57 -17	2.17	28.55	555	
115B	-	-102	-91	107	291	17		31.20	-	
120A	territories .	-102	-91	107	-64	413		26.65	terino.	
120A		102	91	107	64	-413 206	2.17	31.39	200	
120B 120B	_	-202 386	91	104	-68 68	-396 396	2.17	29.84 25.63		
	156					-993		34.41	1	
7.0		10	101		100		100			al coordinates; Wind
1000		fx				ny ma				
_	Туре	(N)	_		Vm) (_			
25 30	Valve	-57 -57			085 6 085 1					
100	Valve	-	-		_	72 -27	-			
105		-65	100000		163 3					
53		215	A01 1					Pi	ipe forces in	al coordinates: Wind
lode		FY	FZ	MX	MY	MZ				
	(N)	(N)	(N)	(Nm)	(Nm)	(Nm)	1			
10	-844 844	-207 207	57 -57	314 -314	184 -195	-43				
10	-844	-207	57	314	195	43	1			
15A	844	207	-57	-314	-631	-1636				
15A	-844	-207	57	314	631	1636				
15B	844 n 7.60	207	-57	-292	-653	-1393				mple2 Sep 12,20

Caepi	pe								Sample Problem 2 Page
-	, ,	بار	/ E	1/E 1			14.6	Pipe for	es in global coordinates: Wind
Node		FY	FZ	MX	MY	MZ	N		1000
150	(N)	(N)	(N)	(Nm)	(Nm)	(Nm)	-		
15B 20A	-430 430	-207 207	57 -57	292 35	653 -653	1393 1094			
20A	23	-207	57	-35	653	-1094	-		
20B	-23	207	-57	136	-644	1085			
20B	337	-48	57	-136	644	-1085	5		
25	-337	48	-57	322	658	1085	_		
30	745	-48	57	-352	2009/52/00	-1085	4		
35 35	-745 853	48 -152	-57 148	367 -204	1298	1085			
40	-853	152	-148	250	1054	662	3		
40	910	-152	148	-250	-1054	-662	6		
45	-910	152	-148	330	1536	662			
45	1075	-152	148	-330	-1536		9		
50	-1075		-148	649	3795	662	1		
35	-65	104	-91	-163	-500	-423	9		
100	65	-104 104	91	163 -163	372 -335	278 -236			
105 110A	-65 65	-104	91	163	332	233			
110A	-65	104	-91	-163	-332	-233	1		
110B	65	-104	91	142	312	224			
110B	67	104	-91	-142	-312	-224			
115A	_	-104	91	-86	312	57	1		
115A		104	-91	86	-312	-57			
115B	-216	-104 102	91	-107 107	291 -291	-17 17	-		
120A	-233	-102	91	-107	-64	-413	8		
120A	and the same of	102	-91	107	64	413	1		
120B	-233	-102	91	-91	-84	-396			
120B		58	-91	91	84	396	1		
125	-413	-58	91	228	-163	993	32		
								Other for	es in global coordinates: Wind
Mada	T	FX	FY	FZ	MX	MY	MZ		
25	Type Valve	(N)	(N) -48	(N) 57	(Nm) -322	(Nm) -658	(Nm) -1085	8	
30	vaive	-669	48	-57	352	1074	1085		
100	Valve	-65	104	-91	-163	-372	-278	Ř	
105		65	-104	91	163	335	236	,	
									Displacements: Wind
SAID SE		10110203	D	lisplacer	ments (global			
Node	X (mm) Y(mm)	Z (mm)	XX	(deg)	YY (deg)	ZZ (deg)	
5	0.021	0.0	00	0.000	0.00	000	0.0067	-0.0003	
10	0.021	0.0	000	0.024	-0.0	004	-0.0069	-0.0004	
15A	0.025	_	349	1.721	-0.0	_	0.0209	-0.0288	
15B	0.360	-	623	1.792	-0.0	$\overline{}$	0.0270	-0.0616	
20A	7.315	_	622	0.115	-0.0	_	0.0485	-0.0654	
20B	7,321	_	511	0.000	-0.0	_	0.0625	-0.0485	
25	2.988	_	551	0.000	-0.0	-	0.0624	-0.0246	
nn.	2.313	_	422	0.000	-0.0	_	0.0617	-0.0235	
_	4 0000	1-0.	362	0.000	-0.0	-	0.0602	-0.0217	
35	1.993	- 6		111111111	1-0.0	r IV	0.0589	-0.0206	
35 40	1.680	-0.	and the latest designation of the latest des	THE RESERVE OF THE PERSON NAMED IN	0.0	100	0.0545	LO DA TE	
35 40 45	1.680 1.152	-0.	205	0.000	-0.0	_	0.0545	-0.0176	
35 40 45 50	1.680 1.152 0.000	-0.0	205	0.000	0.00	000	0.0000	0.0000	
30 35 40 45 50 100	1.680 1.152	0.0	205	0.000		039		-	

Caepi										Page
-			-	Displace	mente /	(alabal)				
Node	X (mm	a Iya	mm)	Z (mm)		(deg)	Y (de	a) Z	Z (dea)	
_	1.993	0.0	-	-1.605	_	_	0.043	_	0.0086	
-	_	0.0	100 mm	-1.744	0.00	3.55	0.030	-	0042	
115A	1.581	0.0	89	-1.363	0.00	084 -	0.005	1 0.	0130	
115B	1.526	0.0	33	-1.332	0.00	95 (.0039	0.	0139	
-	1.525	_	122	-0.499	_	-	.0149		.0070	
	1.464	_	363	-0.429	_	_	,0139	_	.0269	
125	0.000	0.0	00	0.000	0.00	000 0	.0000	0.	0000	
	I I-		Ime	an Im		Luca	Le		Loa	
	Tag F		FY (Z (N)	_	_	_	m) MZ (N	
50 125	-	0	236	\rightarrow	858 71	89 1753	_	16 423	-136 -20	
120	1	U	14	10	0 .	11133	-1	423	Loa	
Mode	Tag 1	- Vino	- 1	Load (N	No of	Total	/Nn		Lua	
20B	mindana ma	Jser ha		207	1	-207	110			
115B	-	Srinnell		1	1	1	\dashv			
							, de		Loa	
Node	Tag /	xial	y She	ar z Sh			Circ.N	4om	Long.Mo	
		N)	(N)	(N)	-		(Nm)		(Nm)	
5		4	944	34	-1	760	-74	_	1939	
								11.	Pipe force	
Node	fx (N)	fy (N)	fz (N)	mx (Nm)	my (Nm)	mz (Nm)	SIF	SL+ (MP		
5	-4	-34	930	-1760	-			13.8	the state of the s	
10	-4	-34	930	-1760			1.00	13.8		
10	-4	-34	365	-1760			1.00	0.2000	3500	
15A	-4	-34	365	-1760	-	196		13.1	-	
15A 15B	-4 -34	-34 4	-224 -224	-1760 972	1057 1674	196	2.54	18.2	0512	
15B	-34	4	-677	972	1674	207	2,04	15.7	-	
20A	-34	4	-677	972	20070000000	183	FU .	16.3	0700	
20A	-34	-1129		972	183	2243	2.54	23.5		
20B	-1129	entransista marro	4	182	-973	2660	2.54	-	and a second	
20B 25	-1168 -1168		4	182 182	973 989	-2660 -1730		21.5 29.6		
30	_	-	4	182	991	-1580	-	27.8	-	
35	-1168	The state of the s	4	182	993	-1507		7207	2000	
35	-1858		-6	136	34	-602	2.49	35.5		
40	-1858	-	-6	136	32	-532		20.2		
40 45	-1858 -1858	-236	-6 -6	136 136	32 29	-532 -407		26.5 29.1		
45	-1858		-6	136	29	-407	2.00	21.8	-	
50	-1858	The second second	-6	136	16	89		32.7	200	
35	10	-5	-616	-905	959	-46		43.7		
100	10	-5	-616	-905	96	-38	_	18.9		
105 110A	10	-5 -5	-484 -484	-905 -905	-111 -124	-36 -36	1.00	26.6	80000	
110A	-	-5	-466	-905	-124	-36	2.17	32.2		
110B		-10	-466	-230	798	-32		40.6		
110B	-5	10	317	-230	-798	32		32.7	0.000	
115A		10	317	-230	-9	7	-	24.6		
115A 115B		10	168	-230	-9 268	7	2.17	27.3 38.2		
	10	5	168	29	1	4	4.17	-	_	
	10	-4	55	29	-268	-4		30.8	25	

Caepi	he							Sample Problem 2	Page 2
Mode	40	6.	fz	Imv	mo:	me	SIF	Pipe forces in local coordinates: Wind 2 L+SO	
Node	(N)	fy (N)	(N)	mx (Nm)	my (Nm)	mz (Nm)		+50 IPa)	
20A	10	4	-276	29	54	-12		7.02	
	6	-9	-276	12	-76	-11	_	5.87	
30.800AS	6	9	481 481	12	76 1803	-20		3.17 9.91	
120	0		101	12	1000	-20	S (Other forces in local coordinates: Wind 2	
		fx	fy	fz	mx	my	mz		
	CONTRACTOR OF THE PARTY OF		(N)	(N)	(Nm)	(Nm)	(Nm)		
25 30	Valve	-1168 -1168	1400000000	4	182 182	989 991	-1730 -1580		
100	Valve	10	-5	-514	-905	96	-38		
105	500000	10	-5	-514	-905	-111	-36		
								Pipe forces in global coordinates: Wind 2	
Node	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)			
5	4	34	-930	1760	_	74	1		
10	-4	-34	930			-68			
10	4	34	-365	1760	1753	68			
15A 15A	4	-34 34	365 224	-1760 1760	1057 -1057	196 -196			
15B	4	-34	-224	-1674	972	207			
15B	4	34	677	1674	-972	-207	1		
20A	-4	-34	-677	2243	972	183			
200.5	4	34 -34	1129		-972	-183			
20B 20B	-4 4	241	-1129 1168	2660 -2660	973 -973	182 -182	1		
25	-4	-241	-1168		989	182			
30	4	241	1168	-1580	-991	-182	1		
35	-4	-241	-1168	_	993	182	-		
35 40	-6 6	236 -236	1858 -1858	-602 532	-34 32	-136 136			
40	-6	236	1858	-532	-32	-136	1		
45	6	-236	-1858		29	136			
45	-6	236	1858	-407	-29	-136			
50 35	10	-236 5	-1858 -616	-89 -905	16 -959	136 -46	1		
20700111	-10	-5	616	905	96	38			
105	10	5	-484	-905	111	-36	1		
110A		-5	484	905	-124	36			
110A 110B	0.775-0.75	5 -5	-466 466	-905 798	124 -230	-36 32			
	10	5	-317	-798	230	-32	1		
115A	-10	-5	317	9	-230	7			
115A		5	-168	-9	230	-7			
115B 115B		-5 4	168 55	-29 29	-268 268	4	1		
120A		-4	-55	-29	-54	-12			
120A	10	4	276	29	54	12	1		
-	-10	-4	-276	-77	7	-11			
120B 125	10 -10	4	481 -481	77 -1753	-7 423	11 20			
	10	7	701	1700	720		200	Other forces in global coordinates: Wind 2	
			FY	FZ	MX	MY	MZ		
Node		(N)	(N)	(N)	(Nm)	(Nm)	(Nm)		
25	Valve	1.7%	241		-1730	-989	-182		
30	76	4	-241	-1168	1580	991	182		

	pe							Sample Pr					Pag
-					2.0	_	ner forces	in global	coordinates	: Wind 2	ă.		
	T	FX FY	FZ		MY M								
100		(N) (N) 10 5	(N) -514	_		m)							
105	valve	-10 -5	514	45000	-96 -3 -111 36	25							
100		-10 -0	1017	300	-11) 05		Dis	solacemer	nts: Wind 2				
- 2			Displacer	ments (o	lobal)		T	procentor	no. Trino E	:			
Node	X (mm) Y (mm)	Z (mm)		leg) YY (deg) ZZ	(deg)						
5	0.000	0.000	0.000	0.000	MARKET MARKET	NAME OF TAXABLE PARTY.	0171						
10	0.000	-0.060	0.251	-0.00	20 -0.0	725 -0.	0172						
15A	0.000	-2.321	11.852	-0.07	94 -0.0	342 -0.	0150						
15B	0.082	-2.410	11.726	-0.10	59 -0.0	322 -0.	0107						
20A	0.910	-2.410	0.544	-0.09	86 -0.0	301 -0.	0058						
20B	0.786	-1.971	0.008	-0.04	61 -0.0	193 -0.	0090						
25	0.047	-0.214	0.005	-0.00	89 -0.0	026 -0.	0049						
30	0.022	-0.124	0.005	-0.00	76 -0.0	019 -0.	0048						
35	0.015	-0.090	0.005	-0.00	56 -0.0	006 -0.	0045						
40	0.012	-0.063	0.004	-0.00		_	0042						
45	800.0	-0.026	0.004	-0.00	33 -0.0	005 -0.	0036						
50	0.000	0.000	0.000	0.000		_	0000						
100	0.015	0.000	0.285	0.035		_	0030						
105	0.015	0.021	0.412	0.038		_	0029						
_	0.015	0.023	0.420	0.039		_	0029						
_	0.022	0.031	0.709	0.066	_		0009						
	0.029	0.031	4,316	0.09	-	-	1003						
-	0.027	0.029	4.681	0.087		-	0006						
_	0.027	-0.007	3.811	0.083	-	_	1002						
	0.027	-0.007	3.484	0.082	-	-	0004						
125	0.000	0.000	0.000	0.000	0.00	00 [0.0	0000	-	22.2				
. Ie									nese				
# Fr		In Cal	1 6 0			I.e.	1.00	Freque	Titules				
71.0	equenc			ipation				otal mass	Truics				
(H	łz)	(second)	Х	Y	Z	Х	Υ	tal mass	livies				
1 1.	tz) 693	(second) 0.5906	X -0.7527	Y 1.9267	Z -1.2144	X 0.0325	Y 0.2127	z 0.0845	lices				
1 1.	tz) 693 462	(second) 0.5906 0.4061	X -0.7527 0.8865	Y 1.9267 -2.1829	-1.2144 -1.5177	X 0.0325 0.0450	9 0.2127 0.2731	0.0845 0.1320	inues				
1 1.1	693 462 671	(second) 0.5906 0.4061 0.3744	X -0.7527 0.8865 -2.4670	Y 1.9267 -2.1829 -1.4160	Z -1.2144 -1.5177 0.2429	X 0.0325 0.0450 0.3488	0.2127 0.2731 0.1149	0.0845 0.0034	TIMES				
1 1.1 2 2.4 3 2.1 4 4.1	693 462 671 054	(second) 0.5906 0.4061 0.3744 0.2467	X -0.7527 0.8865 -2.4670 -0.3463	Y 1.9267 -2.1829 -1.4160 0.3532	-1.2144 -1.5177 0.2429 -1.2605	X 0.0325 0.0450 0.3488 0.0069	V 0.2127 0.2731 0.1149 0.0071	0.0845 0.1320 0.0034 0.0911	Total Control of the				
1 1.0 2 2.0 3 2.0 4 4.0 5 6.0	693 462 671 054	(second) 0.5906 0.4061 0.3744 0.2467 0.1521	X -0.7527 0.8865 -2.4670 -0.3463 1.1232	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279	Z -1.2144 9 -1.5177 0 0.2429 -1.2605 9 0.1158	X 0.0325 0.0450 0.3488 0.0069 0.0723	V 0.2127 0.2731 0.1149 0.0071 0.0605	0.0845 0.1320 0.0034 0.0911 0.0008					
1 1.0 2 2.4 3 2.0 4 4.0 5 6.0	693 462 671 054 574	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894	Z -1.2144 -1.5177 0.2429 -1.2605 0.1158 0.0612	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241	Y 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680	0.0845 0.1320 0.0034 0.0008 0.0008					
1 1.6 2 2.6 3 2.6 3 4 4.6 5 6.6 6 6.7 7 7.6	693 462 671 054 574 771 343	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428	Z -1.2144 9 -1.5177 0.2429 -1.2605 9 0.1158 0.0612 0.1341	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004	Y 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012	0.0845 0.1320 0.0034 0.0008 0.0008 0.0002 0.0010					
1 1.0 2 2.4 3 2.1 3 2.1 4 4.5 5 6.5 6 6.7 7 7.7 8 9.5	693 462 671 054 574 771 343 350	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907	Z -1.2144 9 -1.5177 0.2429 -1.2605 9 0.1158 0.0612 0.1341 -0.1923	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822	9.2127 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012	0.0845 0.0344 0.0034 0.0034 0.0008 0.0002 0.0002 0.0002					
1 1.9 2 2.4 3 2.9 4 4.9 5 6.9 6 6.7 7 7.9 8 9.1	693 462 671 054 574 771 343 350	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907 0.8514	Z -1.2144 0 -1.5177 0 0.2429 -1.2605 0 0.1158 0 0.612 0 0.1341 -0.1923 -0.0625	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002	V 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.0415	0.0845 0.0320 0.0034 0.0034 0.0008 0.0002 0.0010 0.0021 0.0002	nuca				
1 1.1 2 2.4 3 2.1 4 4.1 5 6.6 6 6.7 7 7.1 8 9.1 9 11 10 11	693 462 671 054 574 771 343 350 1.417	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907 0.8514 -0.0892	Z -1.2144 9 -1.5177 0 0.2429 -1.2605 9 0.1158 0 0.0612 0.1341 -0.1923 -0.0625 2 -1.1706	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256	9 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.0415 0.0005	0.0845 0.0845 0.1320 0.0034 0.0911 0.0008 0.0002 0.0010 0.0021 0.0002 0.0785	nuca				
1 1.0 2 2.4 3 2.1 3 2.1 3 2.1 4 4.3 5 6.6 6 6.7 7 7.7 8 9.1 9 11 11 30	693 462 671 054 574 771 343 350 1.417 1.948	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876 0.0837	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685 2.2988	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907 0.8514 -0.0890 0.0522	Z -1.2144) -1.5177) 0.2429 -1.2605) 0.1158 0.0612 0.1341 -0.1923 -0.0625 -1.1706 -0.0056	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256 0.3028	0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.0415 0.0005	0.0845 0.1320 0.0934 0.0911 0.0008 0.0002 0.0010 0.0021 0.0002 0.0785 0.0000	nuca				
1 1.0 2 2.3 3 2.1 3 2.1 3 2.1 4 4.1 5 6.1 6 6.1 7 7.1 8 9.1 11 10 11 11 30 11 51	693 462 671 054 574 771 343 350 1.417 1.948	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685 2.2988	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907 0.8514 -0.0890 0.0522	Z -1.2144 0 -1.5177 0 0.2429 -1.2605 0 0.1158 0 0.612 0.1341 -0.1923 -0.0625 2 -1.1706 0.0564	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256 0.3028 0.0022	9 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.00415 0.0005 0.0002	0.0845 0.1320 0.0034 0.0034 0.0008 0.0002 0.0010 0.0021 0.0002 0.0785 0.0000 0.0002	noca .				
1 1.0 2 2.3 3 2.1 4 4.1 5 6.5 6 6.7 7 7.2 8 9.1 11 10 11 11 30 12 51	693 462 671 054 574 771 343 350 1.417 1.948	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876 0.0837	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685 2.2988	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907 0.8514 -0.0890 0.0522	Z -1.2144) -1.5177) 0.2429 -1.2605) 0.1158 0.0612 0.1341 -0.1923 -0.0625 -1.1706 -0.0056	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256 0.3028 0.0022	9 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.00415 0.0005 0.0002	0.0845 0.0845 0.1320 0.0034 0.0091 0.0008 0.0002 0.0010 0.0002 0.0002 0.0785 0.0000 0.0002 0.0002					
1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1	693 462 671 054 574 771 343 350 1.417 1.948 0.955	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876 0.0837 0.0323 0.0193	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685 2.2988 0.1948	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1428 0.1907 0.8514 -0.0892 0.0522 0.0117	Z -1.2144 -1.5177 0.2429 -1.2605 9.0.1158 0.0612 0.1341 -0.1923 -0.0625 2 -1.1706 0.0547 Total	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256 0.3028 0.0022 0.9430	9 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.00415 0.0005 0.0000 0.0000 0.7818	0.0845 0.1320 0.0034 0.0034 0.0008 0.0002 0.0010 0.0021 0.0002 0.0785 0.0000 0.0002					
1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1	kz) 693 462 671 054 574 771 343 350 1.417 1.948 0.955 1.880	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876 0.0837 0.0323 0.0193	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685 2.2988 0.1948	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1907 0.8514 -0.0892 0.0522 0.0117	Z -1.2144 0 -1.5177 0 0.2429 -1.2605 9 0.1158 0 0.612 0 0.1341 -0.1923 -0.0625 2 -1.1706 0 0.0547 Total	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256 0.3028 0.0022 0.9430	Y 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.00415 0.0005 0.0002 0.0000 0.7818	0.0845 0.0845 0.1320 0.0034 0.0091 0.0008 0.0002 0.0010 0.0002 0.0002 0.0785 0.0000 0.0002 0.0002					
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1 1.1 2 2 2.3 3 2.3 4 4.4 5 6.6 6 6.6 7 7 7.7 8 9.1 110 11 111 30 112 51 113 Node 5 10 115A	kz) 693 462 671 054 677 771 343 350 417 1.948 0.955 1.880 X (mm 0.000 0.000 0.000 0.284	(second) 0.5906 0.4061 0.3744 0.2467 0.1521 0.1477 0.1362 0.1069 0.0876 0.0837 0.0323 0.0193 0.0193 0.000 0.156 6.303 6.590 6.589 6.688	X -0.7527 0.8865 -2.4670 -0.3463 1.1232 -0.6486 -0.0836 1.1979 -0.0592 -0.6685 2.2988 0.1948 Z (mm) 0.000 -0.204 -10.081 -10.046	Y 1.9267 -2.1829 -1.4160 0.3532 -1.0279 -1.0894 0.1907 0.8514 -0.0892 0.0522 0.0117 XX (c 0.000 0.000 0.068 6 0.088	Z -1.2144 0 -1.5177 0 0.2429 -1.6059 0.1158 0.0612 0.1341 -0.1923 -0.0625 0 -1.1706 -0.0056 0 0.0547 Total 0 0 0.05 0 0 0.05 0 0 0.05 0 0 0.05 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	X 0.0325 0.0450 0.3488 0.0069 0.0723 0.0241 0.0004 0.0822 0.0002 0.0256 0.3028 0.0022 0.9430 deg) ZZ 78 0.0 91 0.0 63 0.0 22 0.0 66 0.0 39 0.0	9 0.2127 0.2731 0.1149 0.0071 0.0605 0.0680 0.0012 0.0021 0.0415 0.0005 0.0002 0.7818	0.0845 0.0845 0.1320 0.0034 0.0091 0.0008 0.0002 0.0010 0.0002 0.0002 0.0785 0.0000 0.0002 0.0002					

ecoco In I	pe						Sample Problem 2	Page
- 40					121. a		Mode 1: 1.69 Hz	
Node	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
35	-0.875	1.318	0.000	0.0447	0.0294	0.0139		
10	-0.724	1.089	0.000	0.0427	0.0282	0.0132		
45	-0.479	0.717	0.000	0.0375	0.0248	0.0113		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-0.875	1.038	0.611	0.0382	0.0209	0.0089		
105	-0.875	0.977	0.756	0.0378	0.0203	0.0085		
_	-0.875	0.973	0.766	0.0377	0.0202	0.0084		
-	-0.886	0.952	0.961	0.0299	0.0107	-0.0005		
115A	-0.781	0.952	2.125	0.0247	-0.0065	-0.0016		
_	-0.785	0.941	2.177	0.0209	-0.0139	0.0053		
_	-0.784	0.243	0.893	0.0185	-0.0193	0.0144		
-	-0.735	0.183	0.772	0.0164	-0.0157	0.0171		
_	0.000	0.000	0.000	0.0000	0.0000	0.0000		
120	0.000	10.000	10.000	10.0000	0.0000	0.0000	Mode 2: 2.46 Hz	
Mada I	V /mml	V (mm)	7 (****)	Tyy (dec)	VV /4	77 (4)	mout 2. 2.40 FIZ	
_	X (mm)	Y (mm)	Z (mm)	XX (deg)		The second second second		
_	0.000	0.000	0.000	0.0000	0.0598	-0.0423		
-	0.000	-0.148	-0.212	0.0018	0.0612	-0.0425		
_	0.003	-5.961	-9.681	0.0703	0.0624	-0.0419		
_	0.270	-6.232	-9.455	0.0961	0.0368	-0.0396		
	3.990	-6.229	-0.222	0.0634	-0.0077	-0.0322		
-	4.053	-6.290	-0.005	-0.0213	-0.0262	-0.0191		
25	1.800	-3.186	-0.003	-0.0621	-0.0369	-0.0095		
30	1,400	-2.507	-0.003	-0.0625	-0.0367	-0.0090		
35	1.208	-2.178	-0.003	-0.0626	-0.0362	-0.0083		
40	1.020	-1.850	0.000	-0.0621	-0.0355	-0.0078		
45	0.700	-1.286	0.000	-0.0588	-0.0330	-0.0067		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	1.208	-2.039	-0.794	-0.0611	-0.0279	-0.0038		
105	1.208	-2.013	-0.988	-0.0610	-0.0272	-0.0037		
110A	1.208	-2.011	-1.001	-0.0609	-0.0269	-0.0036		
110B	1.214	-2.002	-1.315	-0.0551	-0.0156	-0.0004		
_	1.268	-2.002	-3.647	-0.0518	0.0103	-0.0046		
	1.302	-1.955	-3.779	-0.0452	0.0220	-0.0157		
-	1.301	-0.412	-1.747	-0.0380	0.0307	-0.0276		
-	1.213	-0.302	-1.529	-0.0341	0.0251	-0.0294		
-	0.000	0.000	0.000	0.0000	0.0000	0.0000		
	2.000	12,020	15.000	10.0000	13.4404	3.0000	Mode 3: 2.67 Hz	
Model	Y (mm)	V (mm)	7 (mm)	VV (doc)	VV (don)	77 (don)	THOUSE OF EIGHT TIE	
Node	X (mm)	Y (mm)	Z (mm)	0.0000		ZZ (deg)		
_	-0.024	0.000	0.000		-0.0052	-0.0517		
_	-0.025	-0.181	0.019	0.0003	-0.0053	-0.0519		
_	-0.030	-4.304	-0.089	0.0107	0.0149	0.0139		
_	-0.473	-4.010	-0.194	0.0057	0.0300	0.0956		
-	-12.484	-4.010	0.086	-0.0052	0.0756	0.1182		
	-12.570	-3.884	0.000	-0.0264	0.1032	0.0873		
_	-5.211	-1.731	0.000	-0.0351	0.1092	0.0448		
30	-4.028	-1.349	0.000	-0.0351	0.1084	0.0430		
35	-3.464	-1.165	0.000	-0.0348	0.1062	0.0397		
40	-2.913	-0.984	0.000	-0.0342	0.1038	0.0376		
45	-1.985	-0.676	0.000	-0.0318	0.0954	0.0322		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-3.464	-1.817	2.410	-0.0351	0.0899	0.0133		
-	-3.464	-1.904	3.038	-0.0351	0.0884	0.0112		

Caepi	p.u.							Page 2
-							Mode 3: 2.67 Hz	
Node	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
110A	-3.464	-1.909	3.078	-0.0351	0.0880	0.0107		
110B	-3.396	-1.887	3.227	-0.0434	0.0683	-0.0321		
115A	-1.387	-1.887	1.454	-0.0355	0.0220	-0.0518		
115B	-1.188	-1.697	1.379	-0.0347	0.0068	-0.0442		
120A	-1.186	0.296	0.698	-0.0001	-0.0172	-0.0087		
120B	-1.161	0.288	0.622	0.0056	-0.0186	0.0171		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000	1	
							Mode 4: 4.05 Hz	
Node	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
5	-0.003	0.000	0.000	0.0000	-0.0050	0.0073		
10	-0.003	0.025	0.018	-0.0001	-0.0051	0.0073		
15A	-0.004	1.206	0.616	-0.0055	-0.0011	0.0112		
15B	-0.099	1.292	0.558	-0.0087	0.0038	0.0164		
20A	-1.838	1.290	-0.050	0.0006	0.0149	0.0155		
20B	-1.807	1.214	-0.004	0.0166	0.0200	0.0103		
25	-0.605	0.253	-0.005	0.0039	0.0111	0.0048		
30	-0.490	0.220	-0.005	0.0021	0.0100	0.0045		
35	-0.443	0.217	-0.005	-0.0015	0.0077	0.0041		
40	-0.399	0.219	-0.004	0.0003	0.0088	0.0039		
45	-0.307	0.197	-0.003	0.0038	0.0106	0.0033		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-0.443	0.161	-0.676	-0.2010	-0.0454	0.0010		
-	-0.443	0.155	-0.996	-0.2010	-0.0434	0.0009		
105		_		_	-0.0445			
110A	-0.443	0.154	-1.017	-0.2194	_	0.0008		
110B	-0.442	0.154	-2.363	-0.3500	-0.0778	-0.0010		
115A	-0.375	0.154	-21,106	-0.4664	0.0046	-0.0017		
_	-0.369	0.159	-22.822	-0.4390	0.0486	-0.0010		
120A	-0.369	0.107	-16.790	-0.3820	0.1098	0.0035		
-	-0.351	0.087	-15.241	-0.3658	0.0994	0.0071		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000		
							Mode 5: 6.57 Hz	
Node	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
5	0.009	0.000	0.000	0.0000	-0.0112	0.0187		
10	0.009	0.066	0.040	-0.0003	-0.0114	0.0188		
15A	0.011	2.309	0.963	-0.0137	0.0067	0.0115		
15B	-0.044	2.369	0.728	-0.0236	0.0237	0.0085		
20A	-2.007	2.360	-0.302	0.0193	0.0636	0.0400		
20B	-1.963	1.929	0.003	0.0867	0.0603	0.0657		
25	1.191	-2.727	0.000	0.0106	0.0126	0.1282		
30	1.302	-2.795	0.000	0.0018	0.0076	0.1309		
35	1.318	-2.762	0.000	-0.0146	-0.0015	0.1358		
40	1.283	-2.637	0.000	-0.0295	-0.0099	0.1286		
45	1.103	-2.209	0.000	-0.0567	-0.0256	0.1103		
50	0.000	0.000	0.000	-0.0000	0.0000	0.0000		
100	1.327	-7.640	-0.015	-0.0111	0.0003	0.1951		
_	1.328	-8.979	-0.012	-0.0108	0.0005	0.1828		
105	W. 10000	-9.063	-0.012	-0.0108	0.0005	0.1020		
-	1.30290	3.000	-	-0.0071	0.0003	-0.1849		
110A	1.328	.0.258	1.0 0.58		4 4 4 1 A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.1043		
110A 110B	1.541	-9.256 -9.268	-0.038	-		0.2952		
110A 110B 115A	1.541 13.907	-9.268	-0.238	-0.0019	0.0095	-0.2853		
110A 110B 115A 115B	1.541 13.907 14.791	-9.268 -8.582	-0.238 -0.193	-0.0019 0.0020	0.0095 0.0130	-0.1086		
115A 115B 120A	1.541 13.907	-9.268	-0.238	-0.0019	0.0095	-		

Caepi	pe						Sample Problem 2	Page
		46 94					Mode 5: 6.57 Hz	
	X (mm)	Y (mm)	Z (mm)	XX (deg)	The second second second	ZZ (deg)		
25	0.000	0.000	0.000	0.0000	0.0000	0.0000		
							Mode 6: 6.77 Hz	
Vode	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
5	0.024	0.000	0.000	0.0000	-0.0032	0.0222		
10	0.024	0.078	0.011	-0.0004	-0.0033	0.0222		
15A	0.029	1.951	0.555	-0.0144	-0.0041	-0.0035		
15B	0.170	1.856	0.471	-0.0174	-0.0027	-0.0287		
-	2.007	1.849	-0.248	0.0163	-0.0053	0.0140		
-	1.596	1,498	0.000	0.0703	-0.0295	0.0654		
25	-0.027	-2.250	0.000	0.0076	-0.0125	0.1576		
30	-0.155	-2.295	0.000	0.0004	-0.0108	0.1616		
35	-0.203	-2.263	0.000	-0.0128	-0.0076	0.1688		
40	-0.233	-2.156	0.000	-0.0248	-0.0044	0.1599		
45	-0.240	-1.803	0.000	-0.0467	0.0018	0.1372		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-0.207	-9.280	-0.203	-0.0106	-0.0077	0.3526		
105	-0.207	-11.771	-0.255	-0.0104	-0.0073	0.3536		
110A	-0.207	-11.934	-0.259	-0.0103	-0.0072	0.3533		
	-1.528	-13.300	-0.308	-0.0062	-0.0012	0.3112		
115A	-11.795	-13.300	-0.470	-0.0007	0.0118	0.1180		
-	-11.845	-13.036	-0.400	0.0054	0.0188	-0.1686		
120A	-11.838	2.845	1.020	0.0192	0.0176	-0.1257		
_	-11.664	2.884	1.008	0.0242	0.0105	0.1562		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000		
			1-	Towns or the			Mode 7: 7.34 Hz	
_	X (mm)	Y (mm)	Z (mm)	XX (deg)		ZZ (deg)		
5	-0.004	0.000	0.000	0.0000	-0.0013	0.0003		
10	-0.004	0.000	0.005	-0.0000	-0.0013	0.0003		
15A	-0.005	0.186	0.076	-0.0007	0.0015	0.0035		
15B	-0.046	0.219	0.048	-0.0019	0.0039	0.0076		
20A	-0.741	0.218	-0.033	0.0015	0.0101	0.0029		
20B	-0.651	0.185	-0.010	0.0064	0.0144	-0.0040		
25	-0.003	-0.012	-0.010	-0.0055	-0.0010	-0.0140		
30	-0.021	0.054	-0.010	-0.0067	-0.0025	-0.0144		
35	-0.041	0.096	-0.010	-0.0092	-0.0055	-0.0152		
40	-0.065	0.135	-0.009	-0.0064	-0.0039	-0.0144		
45	-0.084	0.163	-0.007	-0.0007	-0.0007	-0.0123		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-0.042	0.720	-1.023	-0.2056	-0.0437	-0.0293		
105	-0.042	0.925	-1.315	-0.2200	-0.0379	-0.0287		
-	-0.042	0.938	-1.333	-0.2237	-0.0360	-0.0285		
_	0.018	1.022	-2.380	-0.3090	0.0208	-0.0070		
-	-0.070	1.023	-17.524	-0.3105	0.3231	0.0080		
-	-0.109	0.978	-16.759	-0.1315	0.5067	0.0128		
-	-0.110	0.056	21.139	0.3385	0.4719	0.0110		
71	-0.088	0.022	21.329	0.4901	0.2786	0.0050		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000	Made 0.005 He	
		For a	In a	Love	lance :	lan	Mode 8: 9.35 Hz	
	X (mm)	Y (mm)	Z (mm)	XX (deg)		ZZ (deg)		
5	-0.029	0.000	0.000	0.0000	-0.0228	-0.0221		
10 15A	-0.029	-0.077	0.081	0.0007	-0.0232	-0.0221		
	-0.035	-1.019	0.317	0.0274	0.0495	0.0235		

Caepi	pe						Sample Problem 2	Page
		48 9					Mode 8: 9.35 Hz	
Node	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
15B	-0.411	-0.732	-0.119	0.0070	0.1050	0.0728		
20A	-8.412	-0.727	0.167	-0.0119	0.2666	0.0666		
20B	-6.761	-0.481	-0.010	-0.0486	0.3148	0.0288		
25	8.132	1.869	-0.009	0.0049	0.0071	0.0295		
30	8.054	1.785	-0.009	0.0104	-0.0210	0.0296		
35	7.808	1.704	-0.009	0.0194	-0.0679	0.0296		
40	7.337	1.581	-0.008	0.0260	-0.1031	0.0281		
45	6.019	1.273	-0.007	0.0377	-0.1672	0.0241		
50	0.000	0.000	0.000	0.0000	-0.0000	0.0000		
100	7.820	0.447	-2.988	0.0595	-0.1478	0.0794		
105	7,820	-0.129	-4.029	0.0625	-0.1471	0.0845		
200	7.820	-0.168	-4.096	0.0632	-0.1467	0.0859		
-	7.168	-0.686	-4.281	0.1040	-0.1111	0.2075		
115A	-2.637	-0.684	0.853	0.1161	-0.0554	0.1929		
-	-3.188	-1.064	1.091	0.1051	-0.0334	0.0387		
-	-	and the local division in the local division	-	0.0237	-0.0424	-		
120A	-3.190	0.781	-0.332	_		-0.0263		
	-3.135	0.775	-0.384	0.0062	0.0053	0.0434		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000		
		L	Ta :	L	Lac		Mode 9: 11.42 Hz	
_	X (mm)	Y (mm)	Z (mm)	XX (deg)		ZZ (deg)		
5	0.046	0.000	0.000	0.0000	0.0067	-0.0175		
10	0.046	-0.061	-0.024	0.0011	0.0069	-0.0176		
15A	0.055	-2.502	-0.783	0.0420	0.0004	-0.0185		
15B	0,237	-2.647	-0.441	0.0516	-0.0077	-0.0349		
20A	1.596	-2.618	0.941	-0.0692	-0.0100	0.0426		
20B	0.784	-1.333	-0.005	-0.2485	-0.0475	0.1268		
25	-1.305	10.097	-0.004	0.0458	0.0012	0.2766		
30	-1.270	9.439	-0.004	0.0731	0.0050	0.2831		
35	-1.226	8.922	-0.004	0.1117	0.0101	0.2947		
40	-1.154	8.234	-0.003	0.1433	0.0157	0.2793		
45	-0.951	6.583	-0.003	0.1999	0.0260	0.2395		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-1.223	-2.611	-0.152	0.0535	-0.0150	0.5326		
105	-1.223	-6.336	-0.259	0.0492	-0.0150	0.5209		
	-1.222	-6.576	-0.266	0.0481	-0.0150	0.5164		
-	-2.169	-8.023	-0.222	0.0097	-0.0156	0.0698		
115A	1.894	-8.042	-0.815	-0.0238	-0.0236	-0.1640		
_	2.491	-7.499	-0.888	-0.0256		-0.1217		
	2.501	-0.850	0.271	0.0012	100000000000000000000000000000000000000	-0.1217		
	2.297		-		0.0178			
-	-	-0.574	0.316	0.0066	0.0113	-0.0625		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000	W 1 40 14 05 U-	
							Mode 10: 11.95 Hz	
Node	X (mm)	Y (mm)	Z (mm)	The second second second	PROFESSOR STREET, ST.	ZZ (deg)		
5	-0.005	0.000	0.000	0.0000	-0.0004	-0.0013		
10	-0.005	-0.004	0.000	-0.0000	-0.0004	-0.0013		
15A	-0.006	0.000	0.024	-0.0014	0.0004	0.0027		
15B	-0.044	0.031	0.008	-0.0020	0.0010	0.0071		
20A	-0.689	0.030	-0.094	0.0012	0.0022	0.0026		
20B	-0.667	0.000	-0.074	0.0059	0.0024	-0.0015		
25	-1.767	-0.419	-0.073	0.0052	-0.0522	-0.0060		
30	-2.359	-0.474	-0.073	0.0052	-0.0581	-0.0062		
35	-2.690	-0.501	-0.073	0.0060	-0.0732	-0.0065		
M.M.	21000	0.501	0.010	0.0000	0.0102	0.0000		

Caepi	pe						Sample Problem 2	Page
							Mode 10: 11.95 Hz	
Node	X (mm)	Y (mm)	Z (mm)	XX (deg)	YY (deg)	ZZ (deg)		
40	-2.964	-0.518	-0.068	0.0013	-0.0381	-0.0062		
45	-2.943	-0.480	-0.056	-0.0078	0.0307	-0.0053		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	-2.698	-0.147	-14.621	0.2232	-0.8681	-0.0235		
105	-2.698	0.024	-20.755	0.2392	-0.8679	-0.0250		
110A	-2.699	0.035	-21.155	0.2432	-0.8656	-0.0254		
_	-2.513	0.184	-22.784	0.4827	-0.6537	-0.0593		
-	0.335	0.184	2.252	0.5802	-0.2890	-0.0572		
ment of the	0.504	0.305	3.499	0.5451	-0.1870	-0.0144		
-	0.505	-0.110	-0.266	0.1506	0.0163	0.0095		
-	0.505	-0.125	-0.466	0.0713	0.0629	-0.0051		
-	0.000	0.000	0.000	0.0000	0.0000	0.0000		
120	0.000	10.000	10.000	0.0000	0.0000	0.0000	Mode 11: 30.95 Hz	
	V (1	Iv (max)	7/	Tyv (a.a.)	207 (4-2)	77 (4-2)	Mode 11. 30.33 Hz	
-	X (mm)	Y (mm)	Z (mm)			ZZ (deg)		
5	9.397	0.000	0.000	0.0000	0.0029	0.1125		
10	9.448	0.398	-0.010	-0.0001	0.0029	0.1122		
-	10.713	1.277	-0.024	-0.0025	-0.0061	-0.1880		
15B	12.535	-0.523	0.032	-0.0009	-0.0121	-0.1384		
20A	0.190	-0.557	-0.026	0.0019	-0.0282	0.2355		
20B	-1.317	-0.578	0.000	-0.0015	0.0087	0.1861		
25	-0.078	-0.088	0.000	-0.0098	0.0164	0.0682		
30	0.094	0.017	0.000	-0.0093	0.0147	0.0631		
35	0.162	0.063	0.000	-0.0074	0.0105	0.0539		
40	0.207	0.096	0.000	-0.0054	0.0073	0.0511		
45	0.238	0.123	0.000	-0.0010	0.0002	0.0438		
50	0.000	0.000	0.000	0.0000	0.0000	0.0000		
100	0.165	-0.053	-0.011	-0.0039	-0.0070	-0.0261		
105	0.165	0.138	-0.061	-0.0036	-0.0072	-0.0271		
-	0.165	0.151	-0.065	-0.0036	-0.0072	-0.0271		
-	0.228	0.239	-0.099	0.0001	-0.0052	-0.0053		
_	0.000	0.244	0.004	0.0033	-0.0021	0.0087		
_	-0.027	0.225	0.011	0.0033	-0.0021	0.0038		
-		-				0.0036		
120A	-0.028	0.013	0.000	0.0010	0.0003	212222		
-	-0.024	0.006	0.000	0.0005	0.0006	0.0010		
125	0.000	0.000	0.000	0.0000	0.0000	0.0000		
	***	l.	1	Loren	lear -	lan	Mode 12: 51.88 Hz	
noncontractor.		Y (mm)	Z (mm)	The second division in which the	The second second second second	ZZ (deg)		
5	-0.900	0.000	0.000	0.0000	0.3354	0.1323		
10	-0.905	0.475	-1.218	0.0114	0.3386	0.1310		
15A	-0.902	0.971	-3.949	0.4488	-0.5863	-0.1913		
15B	1.023	-0.831	5.064	0.3657	-0.8969	-0.2592		
20A	4.639	-0.869	2.572	-0.2957	-0.9920	0.3000		
20B	-4.705	0.892	0.457	-0.1382	-0.7667	0.3891		
25	-9.063	0.618	0.245	0.1091	0.9963	0.1566		
30	2.353	-0.595	0.233	0.1075	1.0239	0.1465		
35	7.632	-1.123	0.213	0.0882	0.8393	0.1284		
40	11.583	-1.539	0.197	0.0680	0.6542	0.1217		
45	15.351	-1.914	0.163	0.0125	0.1627	0.1044		
50	0.000	0.000	0.000	-0.0000	-0.0001	0.0000		
100	8.143	-1.095	1.778	-	-0.5018	-0.1460		
-	Automorphic .	-	-	-0.0063	and the latest designation of the latest des	-		
105	8.168 8.170	0.010	-1.938	-0.0133	-0.5338	-0.1623		
110A		880.0	-2.189	-0.0150	-0.5353	-0.1645		

Caepip	pe						Sample Problem 2	Page
			15	5'6			Mode 12: 51.88 Hz	
Node	X (mm)	Y (mm) Z (mm)	XX (deg) YY (deg)	ZZ (deg)		
110B	8.822	0.859	-4.453	0.0366	-0.5116	-0.0141		
115A	0.547	0.888	0.126	0.1285	-0.2177	0.2603		
115B	-0.298	0.233	0.004	0.1539	-0.1085	0.1000		
120A	-0.329	-0.021	0.000	0.0455	0.0502	-0.0380		
120B	-0.406	0.099	0.084	0.0293	0.0532	-0.0117	*2	
125	0.000	0.000	0.000	0.0000	0.0000	0.0000	\$	
							Dynamic susceptibility	
Mode	Frequenc	y Max	ima Nodes	Susceptil	oility			
TO SECOND	(Hz)	*		(psi / ips)	V5.500%			
8	9.350	20A	35	1306				
10	11.948	110		1179	-			
9	11.417	25	35	1051	_			
6	6.771	115		815	\dashv			
12	51.880	45	45	768	-			
5	6.574	120		587	-			
_		15A			ļ:			
3	2.462	20B	2000	445 412				
-		-		-				
1	1.693	15A		404				
4	4.054	115	_	391	-			
7	7.343	120	-	361				
11	30.955	15B	15B	249				
						-	for mode 8: 9.35 Hz, susceptibility = 1306	
		_	ominal Stres		ntensified S			
_	0.0000E+	_	8655E+02	-	.8655E+02	100		
	4.4081E-	_	3788E+02	1.00 1	.3789E+02			
15A	4.2001E-	02 1	6211E+03	2.54 4	.1168E+03			
-	1.6866E-		.0065E+02	2.54 1	.5254E+03			
Annual Contract	3.3123E-		3283E+02	_	.3689E+03			
20B	2.6684E-	01 8	.0485E+02	2.54 2	.0439E+03	ß []		
25	3.2850E-	01 1	1671E+04	1.00 1	.1672E+04			
30	3.2477E-	01 1	1241E+04	1.00 1	.1242E+04			
35	3.1462E-	01 1	0227E+04	2.49 2	5417E+04			
40	2.9550E-	01 7	2098E+03	2.00 1	.4420E+04			
45	2.4219E-	01 7	3521E+03	2.00 1	.4704E+04			
50	0.0000E+	00 1	6167E+04	1.00 1	.6167E+04	14 14		
100	1.1896E-	01 1	9699E+03	1.00 1	.9701E+03			
105	1,5869E-	01 2	2624E+03	1.00 2	.2626E+03			
110A	1.6141E-	01 2	2789E+03	2.17 4	.9347E+03			
110B	3.2871E-	01 2	3953E+03	2.17 5	.1868E+03	6 6		
115A	1.0911E-	01 2	7344E+03	2.17 5	.9211E+03			
	6.0004E-		8775E+03	2.17 6	.2310E+03			
-	3.3412E-	_	4290E+03	and the same of the same of	.0944E+03			
_	1.2802E-	_	6582E+03		.5907E+03			
_	0.0000E+	_	5883E+03		.5883E+03			
weet of I							or mode 10: 11.95 Hz, susceptibility = 1179	
Node	Displacer	nent N	ominal Stree	se SIE III	ntensified S			
_	0.0000E+		3441E+00		.3441E+00			
-	1.8389E-	_	4010E+00		.4012E+00			
-	9.6286E-	-	9989E+01	-	.7774E+02			
15A	1.7480E-	-	1605E+01	-	.3105E+02			
4ED I		U.S. 15	TOTAL STORY	LZ.59	.a 100E#U2			
_	2.7368E-	_	7513E+02		.4475E+02			

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					mode 10: 11.95 Hz, susceptibility = 1179
Node	THE PERSON NAMED IN COLUMN 2 IN COLUMN 2	Nominal Stress	_	Intensified Stress	
25	7.1491E-02	1.8192E+03	-	1.8194E+03	
30	9.4736E-02	2.9409E+03	_	2.9412E+03	
35	1.0774E-01	3.2146E+04	_	7.9894E+04	
10	1.1845E-01	7.2781E+03		1.4556E+04	
45	1.1738E-01	8.5753E+03	-	1.7151E+04	
50	0.0000E+00	1.0196E+04	-	1.0196E+04	
100	5.7564E-01	3.5141E+03	-	3.5144E+03	
105	8.1712E-01	3.6627E+03	_	3.6630E+03	
_	8.3289E-01	3.7927E+03	_	8.2128E+03	
	9.0244E-01	5.9154E+03	_	1.2809E+04	
	8.9626E-02	2.7317E+03		5.9152E+03	
	1,3829E-01	4.1374E+03	-	8.9593E+03	
	1.1331E-02	4.0649E+02	_	8.8021E+02	
-	2.7501E-02	2.9922E+03	_	6.4794E+03	
25	0.0000E+00	1.7837E+03	1.00	1.7837E+03	
	1				mode 9: 11.42 Hz, susceptibility = 1051
		Nominal Stress	_	Intensified Stress	
i	0.0000E+00	5.9140E+01	_	5.9140E+01	
10	2.5930E-03	4.8916E+01	_	4.8921E+01	
15A	1.0323E-01	1.5934E+02	_	4.0465E+02	
5B	1.9716E-02	3.1527E+02	-	8.0062E+02	
20A	7.2931E-02	3.6121E+03	-	9.1730E+03	
20B	6.0866E-02	1.7704E+03	_	4.4961E+03	
25	4.0084E-01	1.2155E+04	_	1.2157E+04	
30	3.7494E-01	9.9628E+03		9.9638E+03	
35	3.5454E-01	1.2155E+04	_	3.0209E+04	
10	3.2733E-01	6,4413E+03	_	1.2883E+04	
15	2.6185E-01	6.3710E+03	-	1.2742E+04	
50	0.0000E+00	1.6735E+04	-	1.6735E+04	
100	1.0299E-01	2.3584E+03	-	2.3587E+03	
105	2.4964E-01	7.0383E+03	_	7.0390E+03	
	2.5911E-01	7.2527E+03	-	1.5705E+04	
_	8.5852E-02	8.4568E+03	-	1.8312E+04	
	8.1185E-02	5.8997E+02	_	1.2775E+03	
-	2.9729E-01	6.7593E+02	-	1.4637E+03	
-	3.5134E-02	3.7925E+02	_	8.2124E+02	
	9.4040E-02	3.2672E+02	_	7.0749E+02	
125	0.0000E+00	1.1955E+U3	1.00	1.1955E+03	
	la.	I	Laur. I		r mode 6: 6.77 Hz, susceptibility = 815
		Nominal Stress	_	Intensified Stress	
5	0.0000E+00	3.8798E+01	_	3.8798E+01	
10	3.0907E-03	2.8052E+01	-	2.8054E+01	
15A	7.9852E-02	4.6307E+02	_	1.1760E+03	
15B	1.9702E-02	2.5632E+02	_	6.5092E+02	
20A	7.9601E-02	1.5013E+03	_	3.8125E+03	
20B	8.6168E-02	5,9256E+02	_	1.5048E+03	
25	8.8607E-02	2.8476E+03	_	2.8479E+03	
90	9.0568E-02	3.0636E+03	_	3.0639E+03	
35	8.9435E-02	7.1612E+03	CONTRACTOR	1.7798E+04	
0	8.5393E-02	2,4994E+03	-	4.9988E+03	
15	7.1604E-02	2.6104E+03	_	5.2207E+03	
50	0.0000E+00	4.9734E+03	14 00	4.9734E+03	

				Dynamic stre	es for mode 6: 6.77 Hz, susceptibility = 815
Mode	Displacement	Nominal Stress	SIF	Intensified Stress	os tar mode o. o. r r raz, subsequantly - o ra
-	3.6545E-01	1.1763E+03	-	1.1764E+03	
_	4.6352E-01	4.0564E+02	-	4.0568E+02	
_	4.6352E-01 4.6994E-01	4.4430E+02	_	9.6209E+02	
_	6.1384E-02	1.1497E+03	-	2.4897E+03	
-	4.6472E-01	5.2877E+03	-	1.1450E+04	
_	5.1346E-01	5.0601E+03	_	1.0957E+04	
-	1.1898E-01	5.9780E+03	-	1.2945E+04	
and the same	4.7470E-01	5.9439E+03	-	1.2871E+04	
-	0.0000E+00	9.5715E+03	-	9.5715E+03	
123	0.0000E+00	9.07 130,403	1.00		s for mode 12: 51.88 Hz, susceptibility = 768
		D	A)E		s for mode 12, 51,66 Hz, susceptibility = 706
_		Nominal Stress		Intensified Stress	
5	0.0000E+00	2.7230E+03		2.7230E+03	
10	5.1476E-02	1.2143E+03	_	1.2144E+03	
_	1.6012E-01	1.6248E+04	-	4.1262E+04	
-	2.0339E-01	1.2088E+04	minoria mana	3.0697E+04	
	2.0883E-01	1.0973E+04	-	2.7865E+04	
-	1.8853E-01	1.4074E+04	-	3.5742E+04	
25	3.5764E-01	4.8964E+04	_	4.8968E+04	
30	9.5551E-02	2.7010E+04	-	2.7013E+04	
35	3.0372E-01	5.6352E+04	-	1.4005E+05	
40	4.6004E-01	4.3307E+04	-	8.6614E+04	
-	6.0907E-01	7.6273E+04	Annual Property lies	1.5255E+05	
_	0.0000E+00	6.7877E+04		6.7877E+04	
_	8.2228E-02	2.4733E+04		2.4735E+04	
-	7.6299E-02	4.6903E+03	-	4.6908E+03	
110A	8.6269E-02	3.9729E+03	2.17	8.6031E+03	
110B	3.8906E-01	1.1674E+04	2.17	2.5280E+04	
115A	2.2095E-02	2.0376E+03	2.17	4.4123E+03	
115B	9.1717E-03	4.7699E+03	-	1.0329E+04	
120A	8.3032E-04	2.8934E+02	-	6.2653E+02	
120B	1.6770E-02	1,1655E+03		2.5238E+03	
125	0.0000E+00	7.6335E+02	1.00	7.6335E+02	10 12-00-00-00 251F 0-00-0
				Dynamic stre	es for mode 5: 6.57 Hz, susceptibility = 587
Node	Displacement	Nominal Stress	SIF	Intensified Stress	
5	0.0000E+00	9.3685E+01	-	9.3685E+01	
10	3.0141E-03	7.8708E+01	-	7.8716E+01	
15A	9.8502E-02	4.2005E+02	2.54	1.0667E+03	
15B	2.8712E-02	6.2902E+01	2.54	1.5974E+02	
20A	7.9916E-02	1.2611E+03	_	3.2026E+03	
20B	1.0836E-01	7.7261E+02	2.54	1.9621E+03	
25	1.1715E-01	3.8865E+03	1.00	3.8869E+03	
30	1.2140E-01	4.2069E+03	1.00	4.2074E+03	
35	1.2048E-01	5.3549E+03	2.49	1.3309E+04	
40	1.1544E-01	3.4466E+03	2.00	6.8933E+03	
45	9.7227E-02	3.6012E+03	2.00	7.2023E+03	
50	0.0000E+00	6.7939E+03	1.00	6.7939E+03	
100	3.0079E-01	3.7529E+03	1.00	3.7532E+03	
	3.5350E-01	6.2165E+03	1.00	6.2171E+03	
105	2 FROSE OS	6.3343E+03	2.17	1.3716E+04	
-	3.5681E-01				
110A	6.0699E-02	6.4210E+03	2.17	1.3904E+04	
110A 110B		6.4210E+03 3.0796E+03	-	1.3904E+04 6.6686E+03	

Caepi	pe			P	Sample Problem 2 Page
	In:	lar v ve	0.1=		ses for mode 5: 6.57 Hz, susceptibility = 587
	THE RESIDENCE OF THE PARTY OF T		SIF	Intensified Stress	
-	1.6843E-01	3.3303E+03	-	7.2115E+03	
_	5.7342E-01	3.2281E+03	_	6.9903E+03	
125	0.0000E+00	9.6135E+03	1.00	9.6135E+03	A
	B	ai i i o	OIE		ses for mode 2: 2.46 Hz, susceptibility = 445
		Nominal Stress		Intensified Stress	
5	0.0000E+00	4.8769E+02	_	4.8769E+02	
10	1.0164E-02 4.4761E-01	4.6294E+02 4.4300E+02	_	4.6298E+02 1.1250E+03	
-	3.7241E-01	4.2039E+02	-	1.0676E+03	
15B 20A	1.5734E-01	1.1884E+03	-	3.0181E+03	
20B	2.9460E-01	1.1004E+03		3.0848E+03	
25	1.4406E-01	2.7066E+02		2.7069E+02	
30	1.1305E-01	1.2266E+02		1.2267E+02	
35	9.8062E-02	1.9762E+02	_	4.9116E+02	
40	8.3168E-02	2.3822E+02	-	4.7644E+02	
45	5.7635E-02	8.5247E+02	microsomers.	1.7049E+03	
50	0.0000E+00	2.6242E+03		2.6242E+03	
100	8.6170E-02	3.0940E+02	_	3.0943E+02	
105	8.8291E-02	3.2991E+02	_	3.2994E+02	
	8.8449E-02	3.3086E+02	-	7.1645E+02	
_	7.0448E-02	6.5222E+01	-	1.4123E+02	
and the same	1.5202E-01	2.0439E+02	-	4.4259E+02	
-	1.6750E-01	3.7891E+02	-	8.2050E+02	
	7.0668E-02	1.4624E+02		3.1666E+02	
_	7.7762E-02	1.2534E+02	-	2.7142E+02	
125	0.0000E+00	1.0460E+03	-	1.0460E+03	
					ses for mode 3: 2.67 Hz, susceptibility = 412
Node	Displacement	Nominal Stress	SIF	Intensified Stress	
5	0.0000E+00	7.8894E+01		7.8894E+01	
10	7.1724E-03	4.6065E+01	1.00	4.6070E+01	
15A	1.6950E-01	1.2467E+03	2.54	3.1659E+03	
15B	2.0141E-02	1.0898E+03	2.54	2.7675E+03	
20A	4.9152E-01	6.3733E+02	2.54	1.6185E+03	
	5.1797E-01	4.9944E+02	2.54	1.2683E+03	
25	2.1618E-01	2.0793E+02	_	2.0795E+02	
30	1.6724E-01	4,3297E+02	1.00	4.3302E+02	
35	1.4390E-01	6.1609E+02	2.49	1.5312E+03	
40	1.2103E-01	6.2420E+02	2.00	1.2484E+03	
45	8.2571E-02	1.5967E+03		3.1934E+03	
50	0.0000E+00	3.5802E+03	1.00	3.5802E+03	
100	1.1885E-01	1.0079E+03	1.00	1.0080E+03	
105	1.4113E-01	1.0155E+03	1.00	1.0156E+03	
	1.4260E-01	1.0134E+03	2.17	2.1944E+03	
110A	2121 may 2 mm 200		0.47	1.5926E+03	
110B	1.8445E-01	7.3546E+02	2.17	100000000000000000000000000000000000000	
110B	AND DESCRIPTION OF THE PERSON NAMED IN	7.3546E+02 2.6771E+02		5.7970E+02	
110B 115A	1.8445E-01		2.17		
110B 115A 115B	1.8445E-01 7.9117E-02	2.6771E+02	2.17 2.17	5.7970E+02	
110B 115A 115B 120A	1.8445E-01 7.9117E-02 8.6092E-02	2.6771E+02 5.9430E+02	2.17 2.17 2.17	5.7970E+02 1.2869E+03	
110B 115A 115B 120A 120B	1.8445E-01 7.9117E-02 8.6092E-02 2.9836E-02	2.6771E+02 5.9430E+02 5.7207E+02	2.17 2.17 2.17 2.17	5.7970E+02 1.2869E+03 1.2388E+03	
110B 115A 115B 120A 120B	1.8445E-01 7.9117E-02 8.6092E-02 2.9836E-02 5.3065E-02	2.6771E+02 5.9430E+02 5.7207E+02 5.6613E+02	2.17 2.17 2.17 2.17	5.7970E+02 1.2869E+03 1.2388E+03 1.2259E+03 1.0213E+03	ises for mode 1: 1.69 Hz, susceptibility = 404
110B 115A 115B 120A 120B 125	1.8445E-01 7.9117E-02 8.6092E-02 2.9836E-02 5.3065E-02 0.0000E+00	2.6771E+02 5.9430E+02 5.7207E+02 5.6613E+02	2.17 2.17 2.17 2.17 1.00	5.7970E+02 1.2869E+03 1.2388E+03 1.2259E+03 1.0213E+03	ses for mode 1: 1.69 Hz, susceptibility = 404

				Dynamic stresse	for mode 1: 1.69 Hz, susceptibility = 404
Node	Displacement	Nominal Stress	SIF	Intensified Stress	
10	1.0118E-02	4.5504E+02	_	4.5509E+02	
15A	4.6808E-01	1.6258E+02	2.54	4.1287E+02	
15B	3.9567E-01	4.1933E+02	-	1.0649E+03	
20A	1.6191E-01	3.0987E+02	_	7.8692E+02	
20B	2.8515E-01	3.9572E+02	-	1.0049E+03	
25	9.7800E-02	5.0584E+02	-	5.0589E+02	
30	7.3581E-02	5,4912E+02	-	5.4918E+02	
35	6.2289E-02	5.7609E+02	-	1.4318E+03	
40	5.1492E-02	5.2290E+02	-	1.0458E+03	
45	3.3953E-02	1.0047E+03	_	2.0093E+03	
50	0.0000E+00	1.3080E+03	-	1.3080E+03	
100	4.7437E-02	2.8532E+02	-	2.8534E+02	
105	4.8638E-02	2.8235E+02	-	2.8238E+02	
	4.8742E-02	2.8217E+02	-	6.1101E+02	
and the last last last	5.1451E-02	2.0437E+02	-	4.4254E+02	
-	8.9150E-02	1.1793E+02	-	2.5536E+02	
	9.3382E-02	2.4363E+02	_	5.2756E+02	
	3.6433E-02	1.1543E+02	_	2.4995E+02	
	4.2571E-02	7.4144E+01	-	1.6055E+02	
125	0.0000E+00	5.8965E+02	_	5.8965E+02	
120	U.0000E+00	3.0903E+02	1.00		or mode 4: 4.05 Hz, susceptibility = 391
N. J.	Di di	In	loir	2000 1000 2000 2000 2000	or mode 4, 4,05 Hz, susceptionity = 391
Node	THE RESIDENCE OF THE PARTY OF T	Nominal Stress	_	Intensified Stress	
5	0.0000E+00	4.1380E+01	_	4.1380E+01	
10	1.2164E-03	3.7748E+01	_	3.7752E+01	
15A	5.3311E-02	1.2157E+02	-	3.0873E+02	
15B	2.2302E-02	8.1329E+01	-	2.0653E+02	
20A	7.2400E-02	2.6278E+02 1.9802E+02	-	6.6733E+02 5.0287E+02	
20B	8.5704E-02		-	CARCING CONTRACTOR CONTRACTOR	
25	2.5836E-02	7.3720E+02	-	7.3727E+02	
30	2.1145E-02	9.1704E+02	-	9.1713E+02	
35	1.9419E-02	2.1803E+03	_	5.4189E+03	
40	1.7914E-02	4.2636E+02	-	8.5273E+02	
45	1.4341E-02	4.3708E+02	-	8.7416E+02	
50	0.0000E+00	9.2899E+02	_	9.2899E+02	
100	2.7345E-02	1.9634E+02	-	1.9636E+02	
105	3.9695E-02	5.8645E+02	_	5.8651E+02	
	4.0508E-02	6.3515E+02	_	1.3754E+03	
	9.4631E-02	4.1279E+03	_	8.9385E+03	
	8.3109E-01	2.4887E+02	-	5.3890E+02	
	8.9853E-01	1.2753E+03	-	2.7616E+03	
	6.6104E-01	8.5948E+01	-	1.8611E+02	
	6.0022E-01	7.2714E+02		1.5745E+03	
125	0.0000E+00	8,0368E+03	1.00	8.0368E+03	
					or mode 7: 7.34 Hz, susceptibility = 361
		Nominal Stress	_	Intensified Stress	
5	0.0000E+00	1.0371E+01	_	1.0371E+01	
10	1.8284E-04	8.5910E+00	_	8.5918E+00	
4-4	7,9260E-03	7.9296E+01	2.54	2.0137E+02	
15A	2.5956E-03	5.4362E+01	2.54	1.3805E+02	
-	ALTERNATION OF THE PARTY.				
15B	2.9204E-02	1.8346E+02	2.54	4.6589E+02	
15A 15B 20A 20B	The second secon	1.8346E+02 4.8951E+01	-	4.6589E+02 1.2431E+02	

Caepi	pe				Sample Problem 2 Page
		11		Dynamic stres	es for mode 7: 7:34 Hz, susceptibility = 361
Node	Displacement	Nominal Stress	SIF	Intensified Stress	
30	2.2965E-03	8.4770E+02	1.00	8.4778E+02	
35	4.1008E-03	2.9204E+03	2.49	7.2583E+03	
40	5.8993E-03	6.7437E+02	2.00	1.3487E+03	
45	7.2325E-03	8.1134E+02	2.00	1.6227E+03	
50	0.0000E+00	7.6143E+02	1.00	7.6143E+02	
100	4.9243E-02	1.5937E+03	1.00	1.5938E+03	
105	6.3294E-02	3.0566E+03	1.00	3.0569E+03	
110A	6.4162E-02	3.1439E+03	2.17	6.8079E+03	
110B	9.3706E-02	3.7530E+03	2.17	8.1267E+03	
115A	6.8994E-01	3.6815E+03	2.17	7.9719E+03	
115B	6.6094E-01	4.0560E+03	2.17	8.7829E+03	
120A	8.3226E-01	4.7999E+03	2.17	1.0394E+04	
120B	8.3975E-01	4.5635E+03	2.17	9.8819E+03	
125	0.0000E+00	1.3997E+04	1.00	1.3997E+04	
110				Dynamic stress	ofor mode 11: 30.95 Hz, susceptibility = 249
Node	Displacement	Nominal Stress	SIF	Intensified Stress	
5	0.0000E+00	1.4673E+02		1.4673E+02	
10	1,5672E-02	3.1503E+02	1.00	3.1506E+02	
15A	5.0303E-02	4.9407E+03	2.54	1.2547E+04	
15B	4.9349E-01	9.4130E+03	2.54	2.3904E+04	
20A	7.5538E-03	7.1967E+02	2.54	1.8276E+03	
20B	5.6624E-02	7.8850E+02	2.54	2.0024E+03	
25	4.6402E-03	4.5602E+02	1.00	4.5607E+02	
30	3.7613E-03	9.6342E+02	1.00	9.6352E+02	
35	6.8264E-03	2.9070E+03	2.49	7.2249E+03	
40	8.9843E-03	8.1499E+02	2.00	1.6300E+03	
45	1.0556E-02	1.1155E+03	2.00	2.2311E+03	
50	0.0000E+00	1.0785E+03	1.00	1.0785E+03	
100	2.1230E-03	9.0906E+02	1.00	9.0915E+02	
105	5.9398E-03	7.0875E+01	1.00	7.0882E+01	
110A	6.4555E-03	1.1909E+02	2.17	2.5787E+02	
110B	9.7885E-03	5.8978E+02	2.17	1.2771E+03	
115A	1.6033E-04	1.1096E+02	2.17	2.4027E+02	
_	8.8499E-03	3.1880E+01	-	6.9034E+01	
-	5.0759E-04	2.5277E+01	-	5.4735E+01	
-	9.7871E-04	2.6086E+01	-	5.6487E+01	
125	0.0000E+00	9.6883E+00	1.00	9.6883E+00	***************************************
					Weight & Center of gravity
120A 120B 125 Empty Insula Conte Lining Total v	5.0759E-04 9.7871E-04	2.5277E+01 2.6086E+01 9.6883E+00 3.2 (kg) 86.05 (kg) 4.28 (kg) 3.5 (kg)	2.17 2.17	5.4735E+01 5.6487E+01	Weight & Center of gravity
		Total weight 741.34, Z = 273	7 32	/mm)	
- 04	130.32, T = 47	41.34, Z=2/3	1.34	(man)	
					Bill of materials: Materials
# Na	ame Description	on			And the first control of the Control
1 31					
22		es Air	200	S 5000	Bill of materials: Pipes
# M	aterial OD	CONTROL DOMESTIC		Total weight	The state of the s
	(mm)	(mm) (mm)	-	(kg)	
1 31	-		6	329.35	
2 31	2 219.07	8.1788 2100		91.344	

	epipe								Sample Problem 2	Page
				100		ii.	70.5		Bill of materials: Pipes	
	Material		Thk	Total I	ength	Total	weight			
		(mm)	(mm)	(mm)		(kg)				
	312	273.05	9.271	18146		1119.	1			
							02		Bill of materials: Bends	
ı	Material	OD	Thk	Radius	Angle	Cour	t Total w	reight		
1		(mm)	(mm)	(mm)	(deg)		(kg)			
	312	168.27			76.04		8.7687			
	312	168.27			90.00	2	20.758			
	312	273.05	9.271	381	90.00	2	73.817		V-40	
								Bi	ill of materials; Reducers	
1	Material	OD1	Thk1	OD2	Thk2	Len	gth Cour	nt Total v	weight	
		(mm)	(mm)		(mm)			(kg)		
	312	273,05	9.271	219.07	8.178	8 530	1	27.676	6	
									Bill of materials: Valves	
	OD	Thk V	Veight	Add.Wei	ight Co	ount T	otal weig	ht		
		(mm) (i	kg)	(kg)		- 0	kg)			
	168.27				1		51.56			
	273.05	9.271 4	59.23	0	1	4	59.23			