

# Tutorial for Fiber Reinforced Piping (FRP) Modeling and Analysis using CAEPIPE

The following are the Steps for FRP Modeling and Analysis using CAEPIPE.

## General

FRP piping has gained wide acceptance in many industries due to its lightweight nature, superior corrosion resistance, temperature capabilities and mechanical strength. Several manufacturers produce different types of FRP pipes and fittings and provide technical assistance to their customers on design matters through installation.

FRP piping can be modeled in CAEPIPE. CAEPIPE will then calculate deflections, element forces & moments, support loads and stresses.

## Tutorial

Snap shot shown below is a sample model for FRP Modeling and Analysis

The screenshot displays the CAEPIPE software interface. On the left is the 'Layout' window showing a data table for the FRP piping model. On the right is the 'Graphics' window showing a 3D isometric view of the piping system, which includes yellow pipes, orange valves, and various fittings.

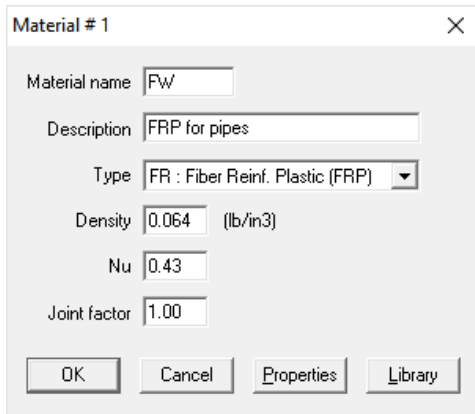
#	Node	Type	DX (ft/in)	DY (ft/in)	DZ (ft/in)	Matl	Sect	Load	Data
1	Title = Tutorial for FRP Piping								
2	10	From	337'8"		210'5-3/4"	-26'4"			Anchor
3	10	Location							Flange
4	20				-3'0-1/8"	FW 24	L1		Anchor
5	30				-2'3-5/8"	FW 24	L1		Flange
6	32	Valve			-0'8-1/4"	CS 24	L1		Flange
7	35				-2'9-1/2"	FW 24	L1		
8	35	Location							
9	38				-1'1-1/4"	FW 24	L1		Flange
10	38	Location							Conc mass
11	39				-0'6-1/4"	FW 24	L1		
12	40	Bend			-2'0"	H12	24F		L1
13	40B	Location							
14	40B	Location							
15	50		2'9"			FW 24	L1		
16	60		0'6"			FW 24	L1		
17	70		0'6"			FW 24	L1		Guide
18	70	Location							Xrestraint
19	80		1'0"			FW 24	L1		
20	90		1'0-1/8"			FW 24	L1		Flange
21	100	Valve	0'8-1/4"			CS 24	L1		Flange
22	100	Location							
23	110		1'3-1/8"			FW 24	L1		Reinf tee
24	120		1'5-1/2"			FW 24	L1		
25	130		0'5"			FW 24	L1		
26	140		0'5"			FW 24	L1		
27	150		0'10"			FW 24	L1		
28	160		0'5"			FW 24	L1		Reinf tee
29	170		0'9"			FW 24	L1		
30	175		0'5"			FW 24	L1		Limit stop
31	175	Location							Restraint
32	180		0'5"			FW 24	L1		
33	190		0'1"			FW 24	L1		
34	200		0'9"			FW 24	L1		
35	210		1'1-1/2"			FW 24	L1		Reinf tee
36	220		3'6-3/8"			FW 24	L1		Limit stop
37	230		3'6-5/8"			FW 24	L1		Reinf tee
38	235		3'6"			FW 24	L1		Limit stop
39	240		3'7"			FW 24	L1		Reinf tee
40	250		1'5-1/2"			FW 24	L1		

### Step 1:

First define FRP materials required for piping system through Layout window > Misc > Materials. In the Material List window shown on the screen, double click on an empty row to input a new material or on a material description to edit the material properties.

### Step 2:

In the Material dialog shown, enter the FRP material properties as given below.

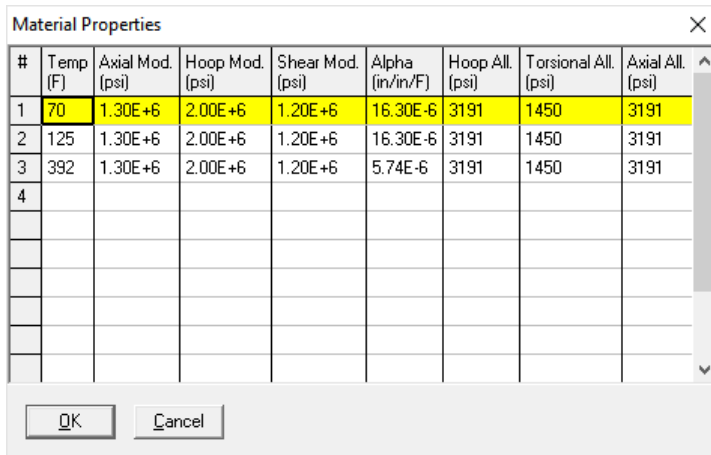


Material # 1 dialog box showing input fields for Material name (FW), Description (FRP for pipes), Type (FR : Fiber Reinf. Plastic (FRP)), Density (0.064 lb/in3), Nu (0.43), and Joint factor (1.00). Buttons for OK, Cancel, Properties, and Library are at the bottom.

The material name can be up to five alpha-numeric characters. Enter description, density and Poisson's ratio. You need to select "FR: Fiber Reinf. Plastic (FRP)" from the Type drop-down combo box before you click on the Properties button.

### Step 3:

Click on the Properties button, you are shown the table below where you can enter temperature-dependent properties. Additionally, you can also define the Hoop, Torsional and Axial allowable stresses so that CAEPIPE can use them to compare with calculated stresses under the FRP "Sorted Stresses" results.

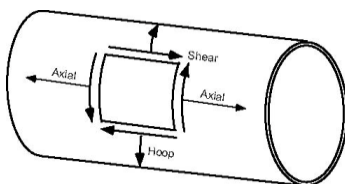


Material Properties dialog box showing a table with columns: #, Temp (F), Axial Mod. (psi), Hoop Mod. (psi), Shear Mod. (psi), Alpha (in/in/F), Hoop All. (psi), Torsional All. (psi), and Axial All. (psi). The table contains three rows of data.

#	Temp (F)	Axial Mod. (psi)	Hoop Mod. (psi)	Shear Mod. (psi)	Alpha (in/in/F)	Hoop All. (psi)	Torsional All. (psi)	Axial All. (psi)
1	70	1.30E+6	2.00E+6	1.20E+6	16.30E-6	3191	1450	3191
2	125	1.30E+6	2.00E+6	1.20E+6	16.30E-6	3191	1450	3191
3	392	1.30E+6	2.00E+6	1.20E+6	5.74E-6	3191	1450	3191
4								

### FRP Material Moduli

CAEPIPE requires three moduli for the FRP material:



- Axial or Longitudinal (this is the most important one)
- Hoop (used in Bourdon effect calculations). If this modulus is not available, use axial modulus.

- Shear or Torsional. If this modulus is not available, use engineering judgment in specifying 1/2 of axial modulus or a similar value. Note that a high modulus will result in high stresses, and a low modulus will result in high deflections.

For FRP bends, a Flexibility factor of 1.0 is used unless you override it by specifying a Flexibility factor inside the bend dialog. Also for FRP bends, CAEPIPE uses a default SIF of 2.3. You can override this too by specifying User-SIFs at the bend end nodes (A and B nodes).

**Step 4:**

After defining the FRP material properties, Section Properties and Loads required for the stress analysis, complete the stress layout. Save the model and Analyze through Layout window > File > Analyze.

**Step 5:**

Upon successful analysis, CAEPIPE will show the calculated stresses, deflections, support loads, element forces and support load summary. Each item can be seen under the respective title in Results. FRP element stresses can be seen, sorted or unsorted.

#	Hoop				Max Long				Min Long				Torsion			
	Node	Stress (psi)	Allow (psi)	Stress/Allow	Node	Stress (psi)	Allow (psi)	Stress/Allow	Node	Stress (psi)	Allow (psi)	Stress/Allow	Node	Stress (psi)	Allow (psi)	Stress/Allow
1	20	3537	3191	1.11	160	8718	3191	2.73	110	-7437	3191	2.33	1110	1043	1450	0.72
2	20	3537	3191	1.11	1170	8537	3191	2.68	160	-7347	3191	2.30	1100	1043	1450	0.72
3	30	3537	3191	1.11	1160B	3611	1450	2.49	110	-6837	3191	2.14	1140	698	1450	0.48
4	1270	3537	3191	1.11	40A	3531	1450	2.43	1160B	-2735	1450	1.89	1120	698	1450	0.48
5	1235	3537	3191	1.11	1160A	2839	1450	1.96	40A	-2651	1450	1.83	1130	698	1450	0.48
6	220	3537	3191	1.11	110	6119	3191	1.92	1170	-5673	3191	1.78	1145	698	1450	0.48
7	250	3537	3191	1.11	2080	5945	3191	1.86	160	-4934	3191	1.55	1150B	624	1450	0.43
8	1230	3537	3191	1.11	38	5628	3191	1.76	160	-4241	3191	1.33	1155	624	1450	0.43
9	32	3537	3191	1.11	38	5628	3191	1.76	1230	-4136	3191	1.30	1110	509	1450	0.35
10	200	3537	3191	1.11	1150A	2364	1450	1.63	110	-4128	3191	1.29	1792	467	1450	0.32
11	35	3537	3191	1.11	40B	2317	1450	1.60	1230	-4065	3191	1.27	1792	467	1450	0.32
12	235	3537	3191	1.11	2080	4814	3191	1.51	1160A	-1816	1450	1.25	1790B	467	1450	0.32
13	35	3537	3191	1.11	1790A	2182	1450	1.50	38	-3625	3191	1.14	2080	460	1450	0.32

#	Node	Hoop (psi)	Axial (psi)	Bending (psi)	Longitudinal Max (psi)	Longitudinal Min (psi)	Torsional (psi)
1	10	3537	-1408	33	-1375	-1441	0
	20	3537	-1408	21	-1387	-1429	0
2	20	3537	1001	2702	3703	-1701	70
	30	3537	1001	1294	2295	-293	70
3	32	3537	1001	410	1411	591	70
	35	3537	1001	2004	3005	-1003	70
4	35	3537	1001	2004	3005	-1003	70
	38	3537	1001	4626	5628	-3625	70
5	38	3537	1001	4626	5628	-3625	70
	39	3537	1001	3310	4311	-2309	70
6	40A	1504	440	3091	3531	-2651	29
	40B	1504	588	1729	2317	-1141	2
7	40B	3537	1365	1851	3216	-486	5
	50	3537	1365	718	2083	648	5
8	50	3537	1365	718	2083	648	5
	60	3537	1365	248	1613	1118	5

CAEPIPE : Displacements: Operating (W+P1+T1) - [FRP\_Piping.res...

#	Node	Displacements (global)					
		X (inch)	Y (inch)	Z (inch)	XX (deg)	YY (deg)	ZZ (deg)
1	10	0.000	0.000	0.000	0.0000	0.0000	0.0000
2	20	0.000	0.000	0.000	0.0000	0.0000	0.0000
3	30	-0.068	-0.012	-0.051	-0.0238	0.1723	0.0076
4	32	-0.093	-0.015	-0.069	-0.0238	0.1726	0.0077
5	35	-0.198	-0.027	-0.131	-0.0088	0.0676	0.0168
6	38	-0.210	-0.028	-0.156	-0.0004	-0.0487	0.0205
7	39	-0.206	-0.027	-0.167	0.0033	-0.1183	0.0222
8	40A	-0.206	-0.027	-0.167	0.0033	-0.1183	0.0222
9	40B	-0.045	-0.011	-0.138	0.0064	-0.2673	0.0274
10	50	-0.026	-0.006	-0.081	0.0066	-0.3085	0.0240
11	60	-0.013	-0.003	-0.040	0.0067	-0.3153	0.0197
12	70	0.000	0.000	0.000	0.0068	-0.3056	0.0137
13	80	-0.001	0.000	0.061	0.0070	-0.2687	0.0027

CAEPIPE : Loads on Anchors: Operating (W+P1+T1) - [FRP\_Piping...

#	Node	Tag	FX (lb)	FY (lb)	FZ (lb)	MX (ft-lb)	MY (ft-lb)	MZ (ft-lb)
1	10	1	-426	62939	-205	0	0	0
2	20		-7988	-2515	-47736	-4353	26387	1396
3	590		-103	651	-1459	-372	-50	-94
4	890		-28	233	448	-207	-14	-17
5	990		-10	281	207	-226	-5	-1
6	1090		-1	345	-98	-251	-1	2
7	1100		-1359	770	-995	-394	-1030	-4511
8	1410	16	-1280	-498	-1328	-23	-67	
9	1510	-13	-1154	-449	-1211	20	59	
10	1710	-8	-1095	-403	-1042	16	39	
11	1910	10	-1057	-393	-1029	-16	-45	
12	2000		605	1244	-689	-318	1680	940

CAEPIPE : FRP forces in local coordinates: Operating (W+P1+T1) - ...

#	Node	fx (lb)	fy (lb)	fz (lb)	mx (ft-lb)	my (ft-lb)	mz (ft-lb)	SIF
1	10	-62939	-409	1	0	0	-205	1.60
2	20	-15202	-2106	-7987	-1396	26390	-4558	
3	30	-15202	-1480	-7987	-1396	8003	-431	1.60
4	32	-15202	-869	-7987	-1396	2512	376	1.60
5	35	-15202	-110	-7987	-1396	-19786	1743	
6	38	-15202	244	-7987	-1396	-28605	1699	1.60
7	39	-15202	386	-7987	-1396	-32765	1535	1.60
8	40A	-15202	-7987	-386	-1396	1535	32765	2.30
9	40B	-7987	15202	-1294	103	-532	18336	2.30
10	40B	-7987	1294	15202	103	-18336	-532	
11	50	-7987	1498	15202	103	-6934	-1579	
12	50	-7987	1498	15202	103	-6934	-1579	
13	60	-7987	1534	15202	103	-667	-2361	

CAEPIPE : Support load summary for anchor at node 10 - [FRP\_...

Load combination	FX (lb)	FY (lb)	FZ (lb)	MX (ft-lb)	MY (ft-lb)	MZ (ft-lb)
Sustained	0	-426	0	-205	0	0
Operating1	1	-426	62939	-205	0	0
Sustained+Seismic	36	-408	36	-197	17	0
Sustained-Seismic	-36	-444	-36	-214	-17	0
Operating1+Seismic	37	-408	62974	-197	17	0
Operating1-Seismic	-35	-444	62903	-214	-18	0
Maximum	37	-408	62974	-197	17	0
Minimum	-36	-444	-36	-214	-18	0
Allowables	0	0	0	0	0	0

Stiffness matrix formulated internally in CAEPIPE and the formulas used for computing different stresses are given below for quick reference.

**Stiffness matrix**

The stiffness matrix for a pipe is calculated using the following terms:

Axial term =  $L / EA$

Shear term = shape factor x  $L / GA$

Bending term =  $L / EI$

Torsion term =  $L / 2GI$

where L = length, A = area, I = moment of inertia, E = elastic modulus, G = shear modulus

**For an isotropic material**,  $G = E / 2(1 + \nu)$ , where  $\nu$  = Poisson's ratio,

**For a FRP material**, E = axial modulus and G is independently specified (i.e., it is not calculated using E and  $\nu$ ).

The hoop modulus and FRP Poisson's ratio are only used in Bourdon effect calculation where,

Poisson's ratio used = FRP Poisson's ratio input x (axial modulus / hoop modulus)

## **FRP Stresses**

$$\text{Hoop stress: } S_H = \frac{PD}{2t_m}$$

$$\text{Axial stress: } S_A = \frac{PD}{4t_m} + \frac{F}{A}$$

$$\text{Bending stress: } S_B = \frac{\sqrt{(i_i M_i)^2 + (i_o M_o)^2}}{Z}$$

$$\text{Torsional stress: } S_T = \frac{M_t}{2Z}$$

$$\text{Longitudinal maximum} = \text{Axial} + \text{Bending} = S_A + S_B$$

$$\text{Longitudinal Minimum} = \text{Axial} - \text{Bending} = S_A - S_B$$

where

$P$  = pressure

$D$  = outside diameter

$t_m$  = minimum thickness

= nominal thickness x (1 - mill tolerance/100) - corrosion allowance

$i_i$  = in-plane stress intensification factor

$i_o$  = out-of-plane stress intensification factor

$M_i$  = in-plane bending moment

$M_o$  = out-of-plane bending moment

$M_t$  = torque

$Z$  = section modulus

$F$  = axial force

$A$  = cross-section area